

GIGANTISM IN SHIPBUILDING AND CORRELATIVE SAFETY REQUIREMENTS

**LE RENDEZ-VOUS DE L'ASSURANCE TRANSPORTS - CANNES
28 ET 29 AVRIL 2009**

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Bureau Veritas – Marine Division – Paris

- **Economy of scale: less carrying cost per unit of cargo or passenger**
- Imperative to ensure a sufficient filling ratio
- Reduced flexibility is a disadvantage:
 - Reduced number of port facilities
 - Shortage of docking facilities
 - Not allowed in Panama & Suez canals. Malacca strait in the future?
- Volume of casualties

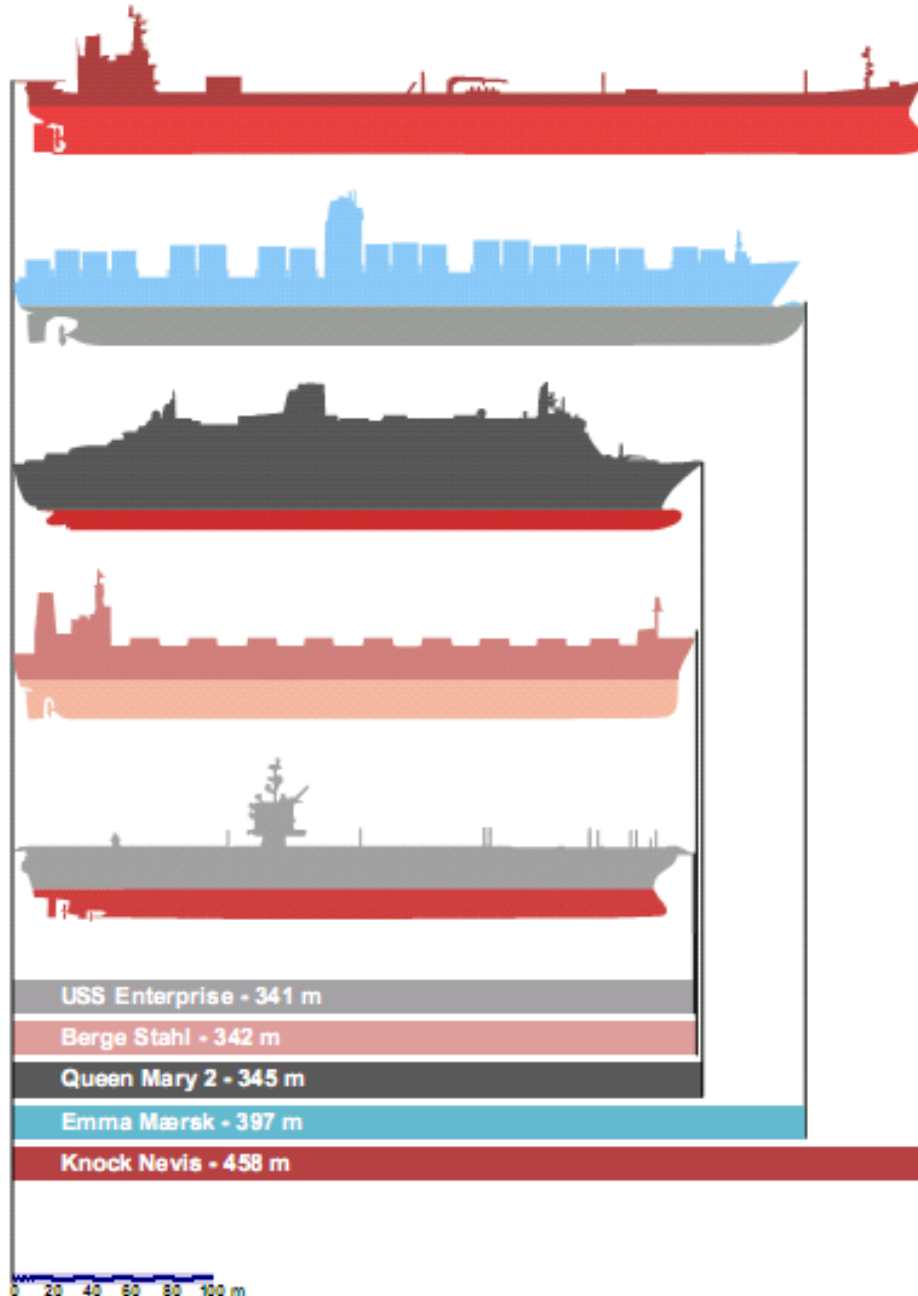


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SHEER SIZE



LE RENDEZ-VOUS DE CANNES



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28 ET 29 AVRIL 2009



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LE
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DE CANNES

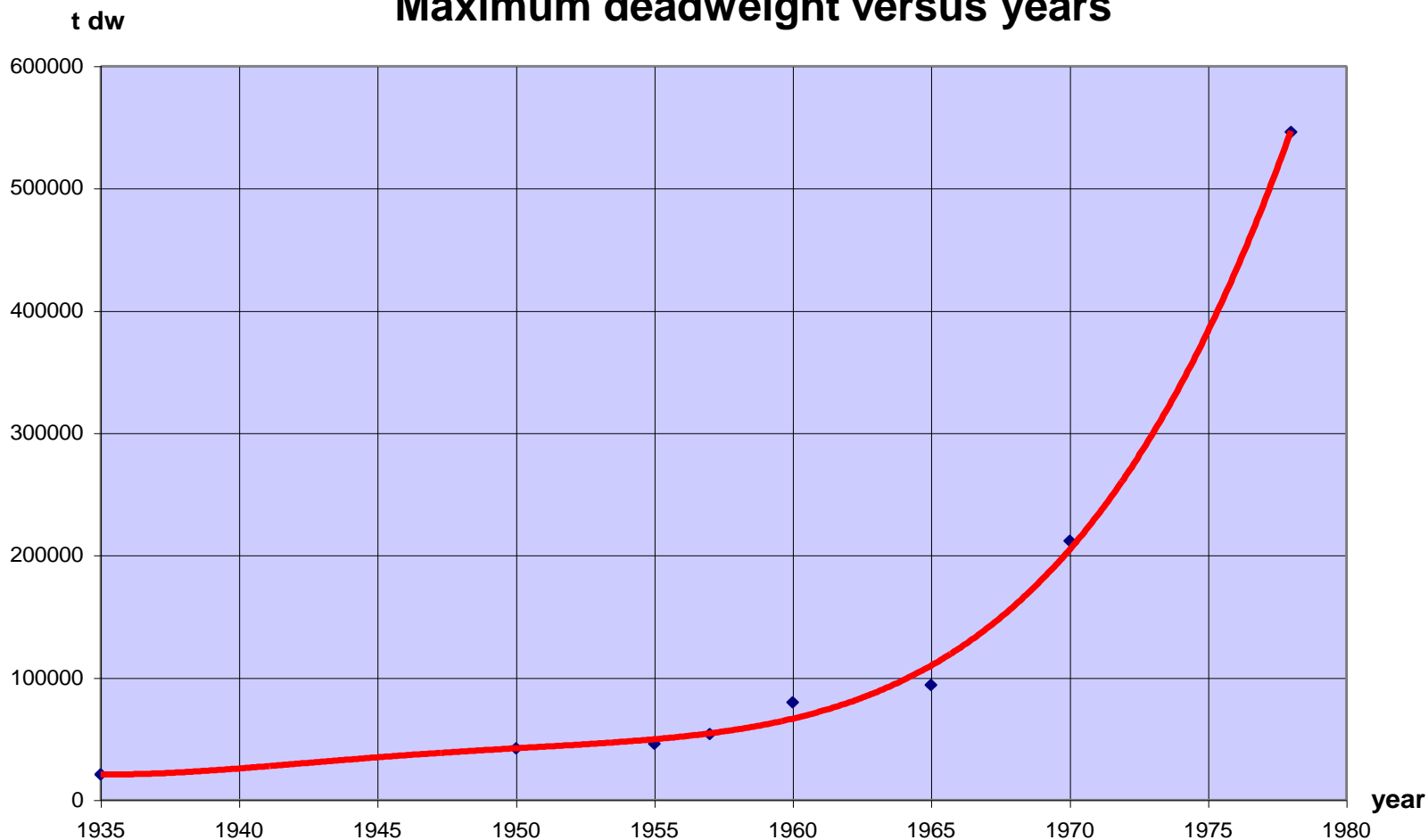
CONCERNED SHIPS

- 1. Tankers**
- 2. Bulk carriers**
- 3. Container ships**
- 4. Cruise-liners**



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Tankers built in France from 1935 to 1980 Maximum deadweight versus years



and studies for 1,000,000 tdw tankers

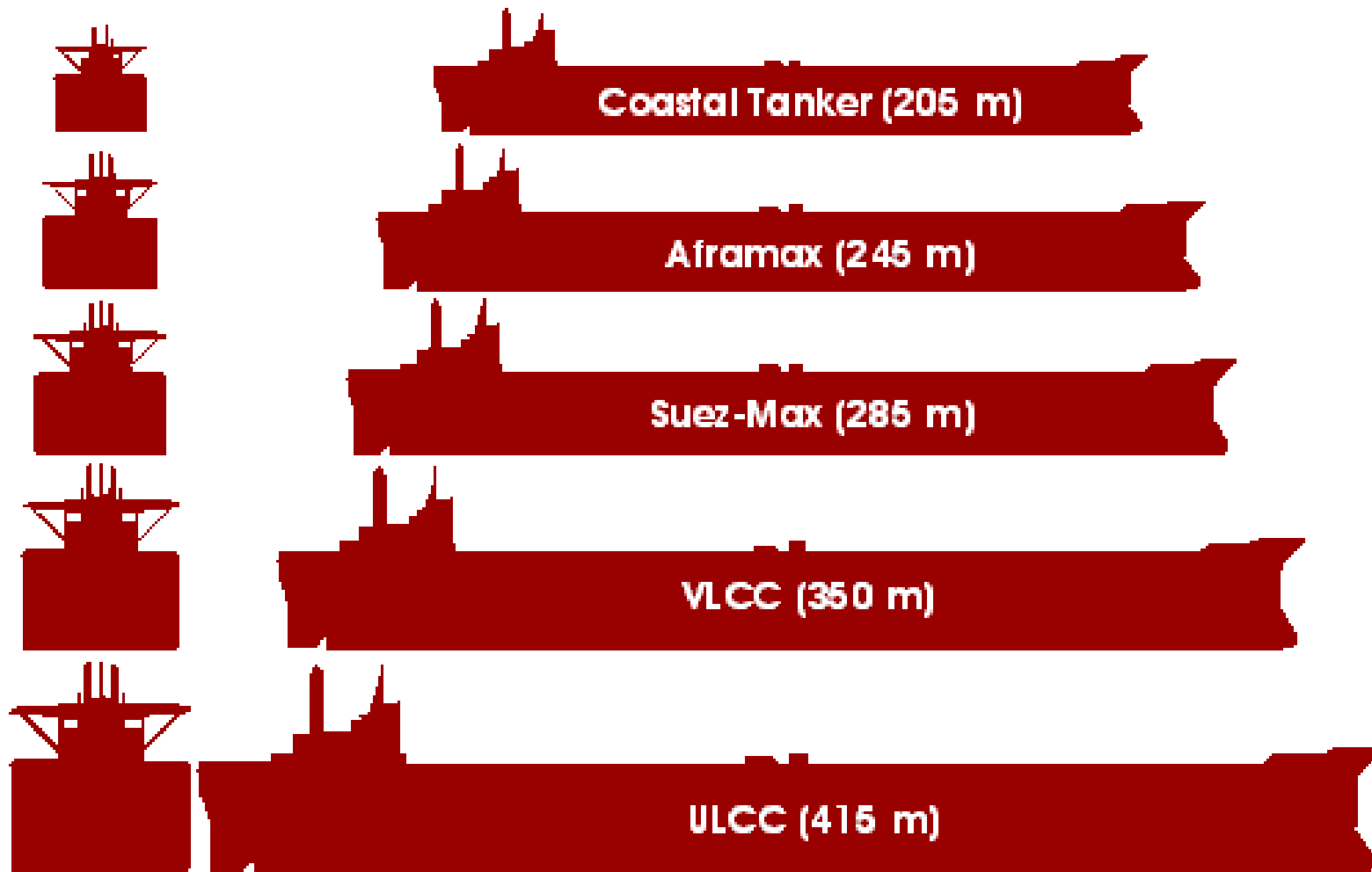


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TANKERS



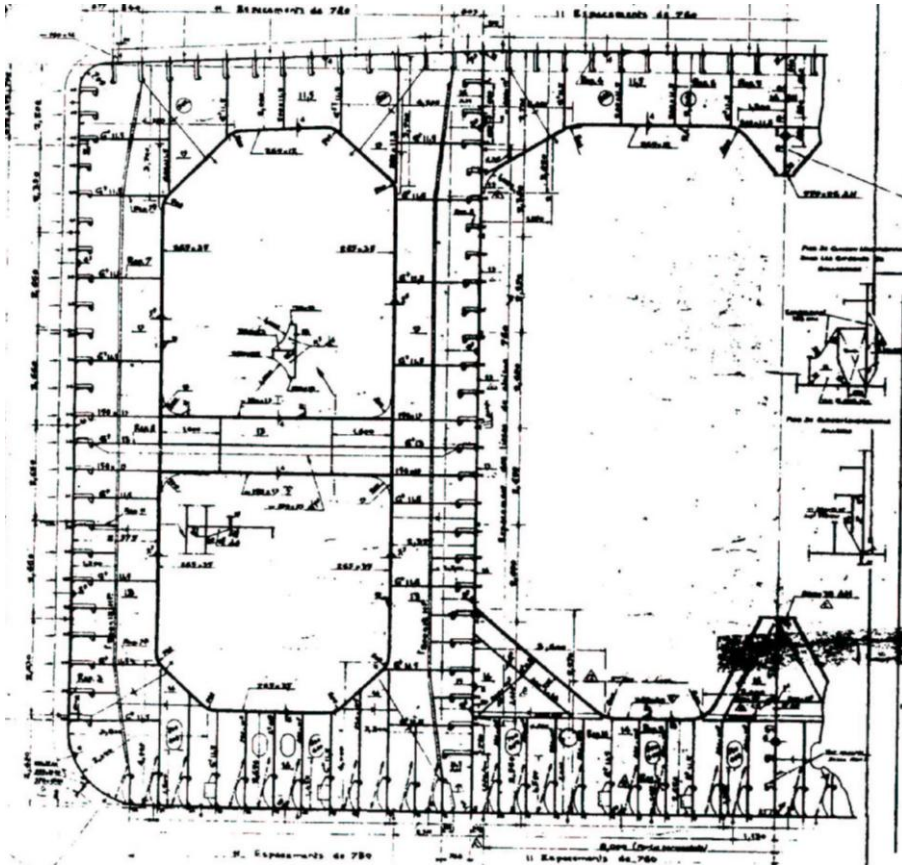
LE
RENDEZ-VOUS
DE CANNES



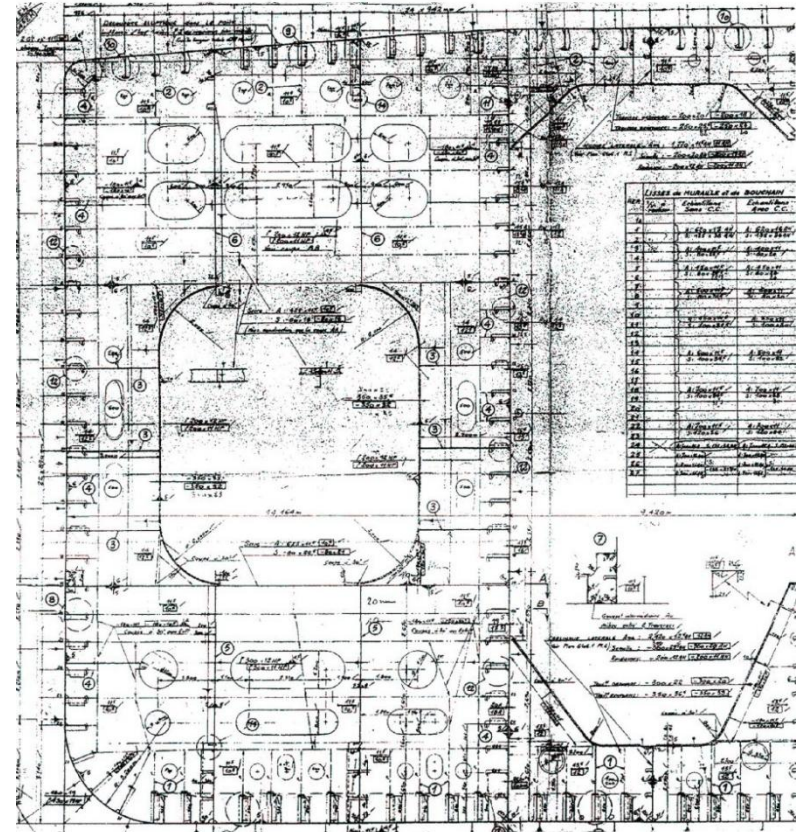
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Bételgeuse : 120 000 tdw

Magdala : 211 000 tdw



L = 268.66 m B = 38.92 m D = 20.35 m d = 15.087 m
Bottom thickness = 26 mm DH



L = 307.47 m B = 47.17 m D = 24.5 m d = 17.68 m
Bottom thickness = 27 mm DH

TANKERS

Batillus : 550 000 t - CA 1976 for Shell



TANKERS

Batillus & Nordic Clansman





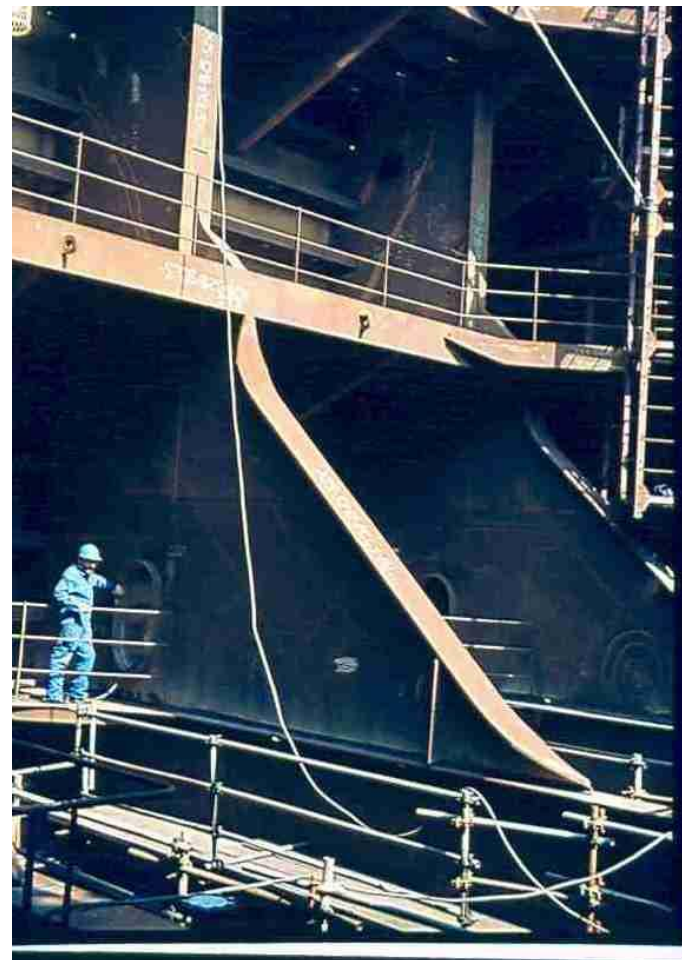
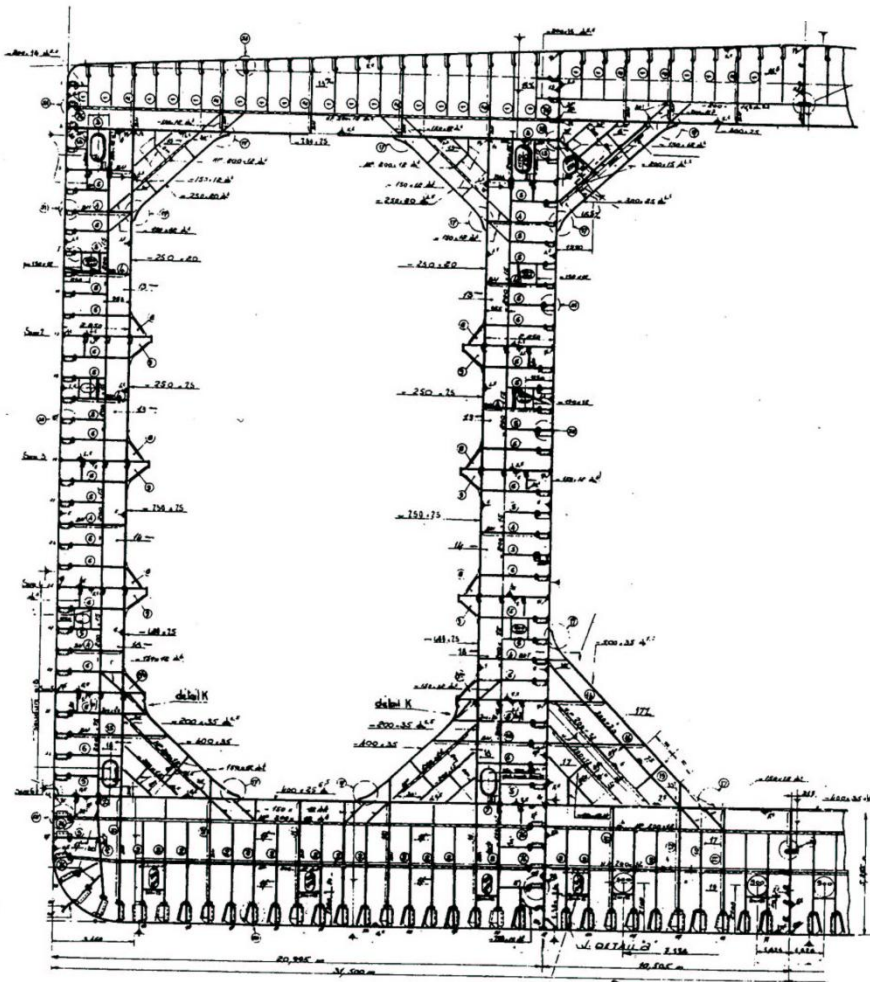
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TANKERS



LE RENDEZ-VOUS DE CANNES

Batillus : 550,000 tdw



L = 414.22 m B = 63 m D = 35.9 m d = 28.6 m

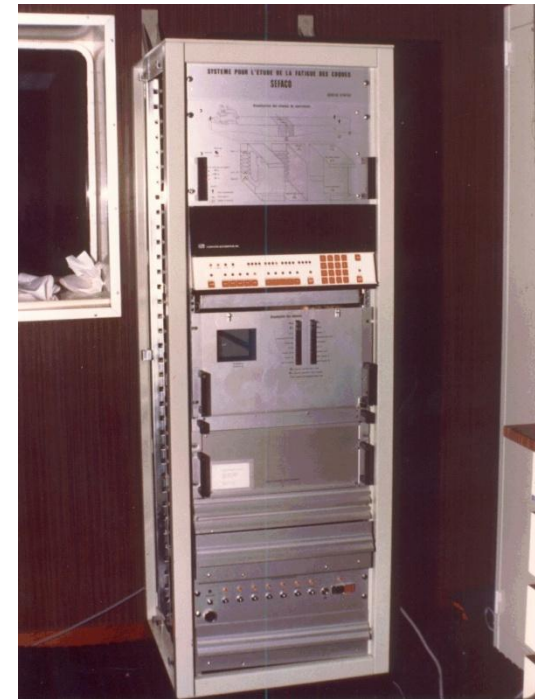
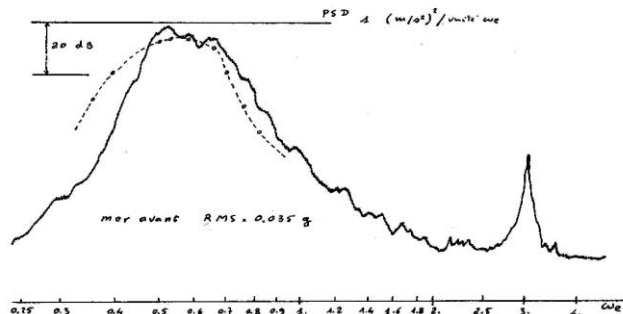
Bottom thickness = 27,5 mm DH Side shell thickness = 25 m



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Technical structural challenges

- **Magdala: shear buckling during tank tests**
solved by measurements and stress computation (first time)
- **300,000 tdw with HS steel: early fatigue cracking**
solved by fatigue tests, detail new designs
- **550,000 tdw: springing phenomenon**
solved by ship behaviour and structural response computation
verified by hull stress monitoring





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TANKERS



LE
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DE CANNES

550,000 tdw operational safety



Stop length > 2 miles - Turning circle diameter > 1 mile



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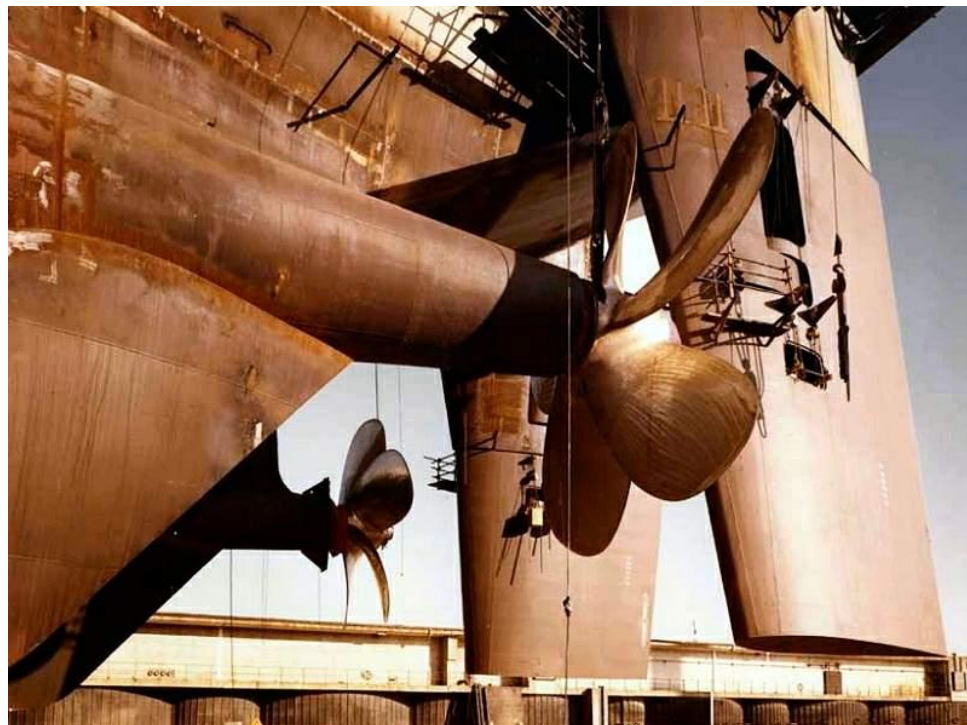
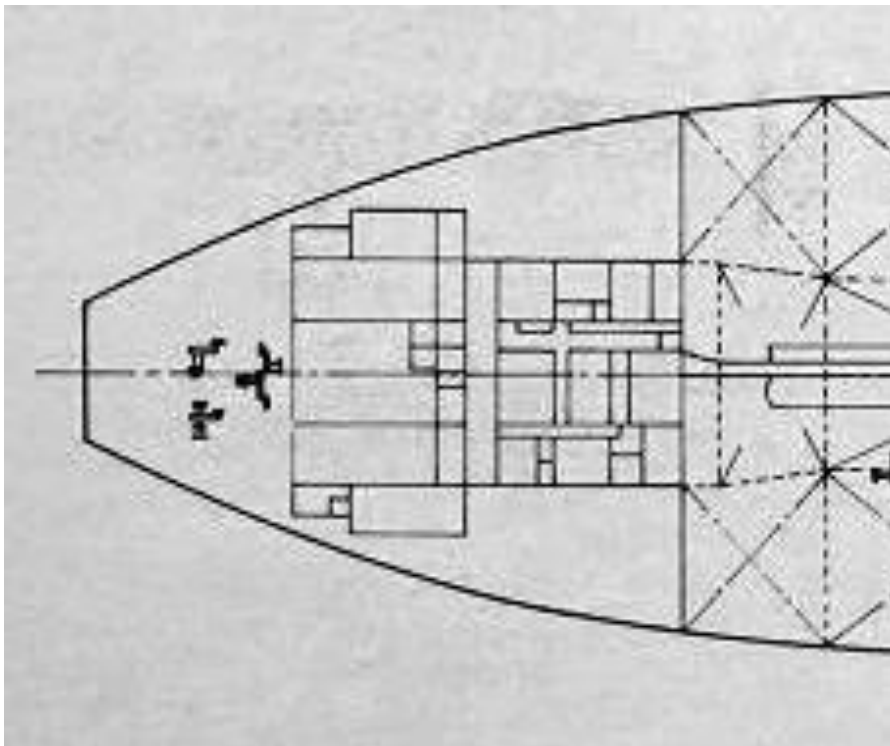
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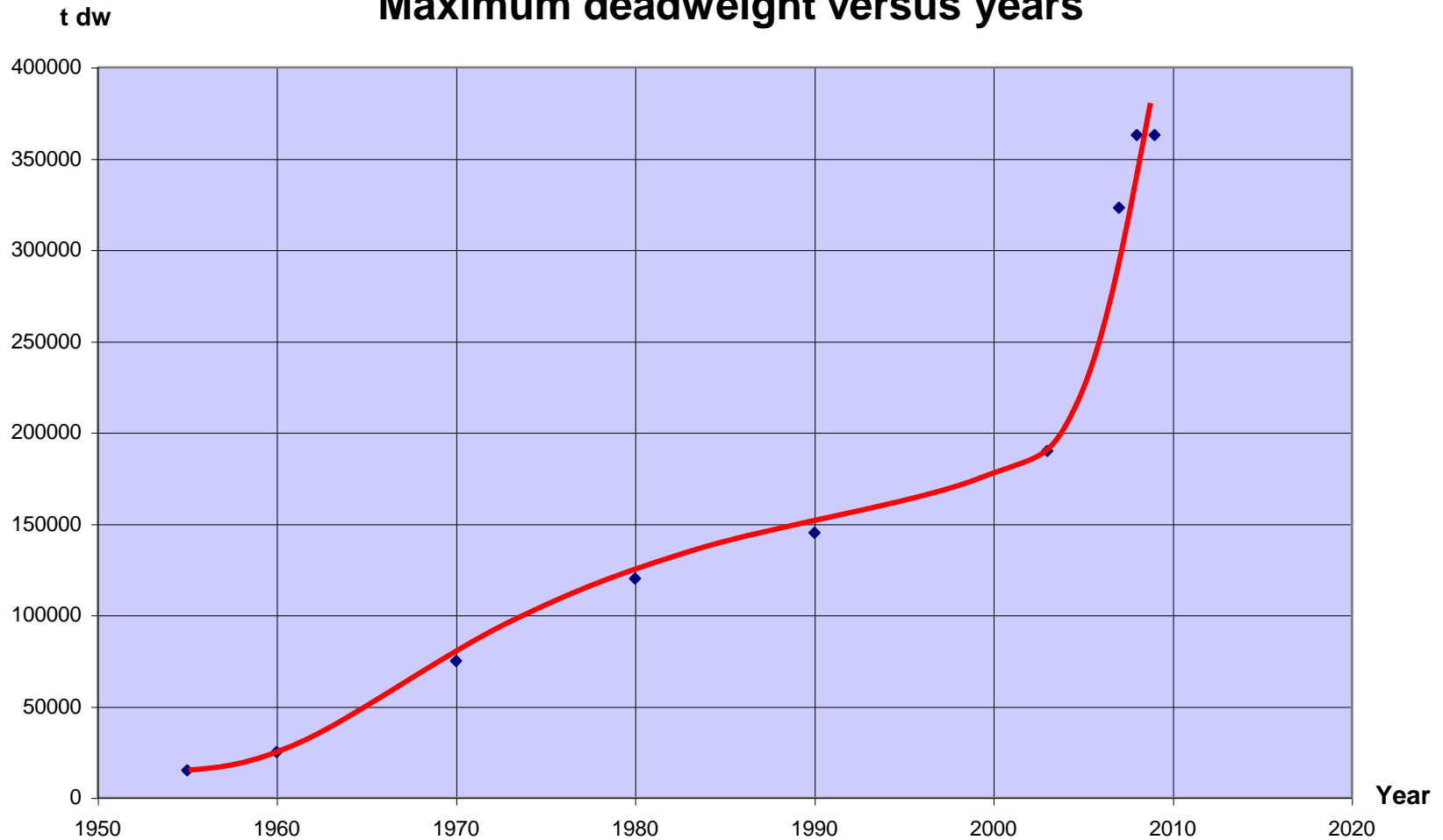
550,000 tdw operational safety

two independant engine rooms

two propellers, two rudders



Bulk carriers built from 1955 to 2007 Maximum deadweight versus years



BULK CARRIERS

Berge Stahl 364,000 tdw (9 ships)



Very Large Ore Carriers (VLOC)



MAIN PARTICULARS:	
L.O.A.	327.00m
B.MLD	55.00m
D.MLD.	29.00m
Summer Draft	21.40m
Gross Tonnage	152,305T
Net Tonnage	55,601T
Deadweight	297,592T
Speed	atb. 14.5Knots
MAIN ENGINE:	
MAN B&W 6S80MC-C Mk7	1set
M.C.O.	22,360kW(BHP)*73rpm
NOR.O.	19,000kW(BHP)*abt.69rpm

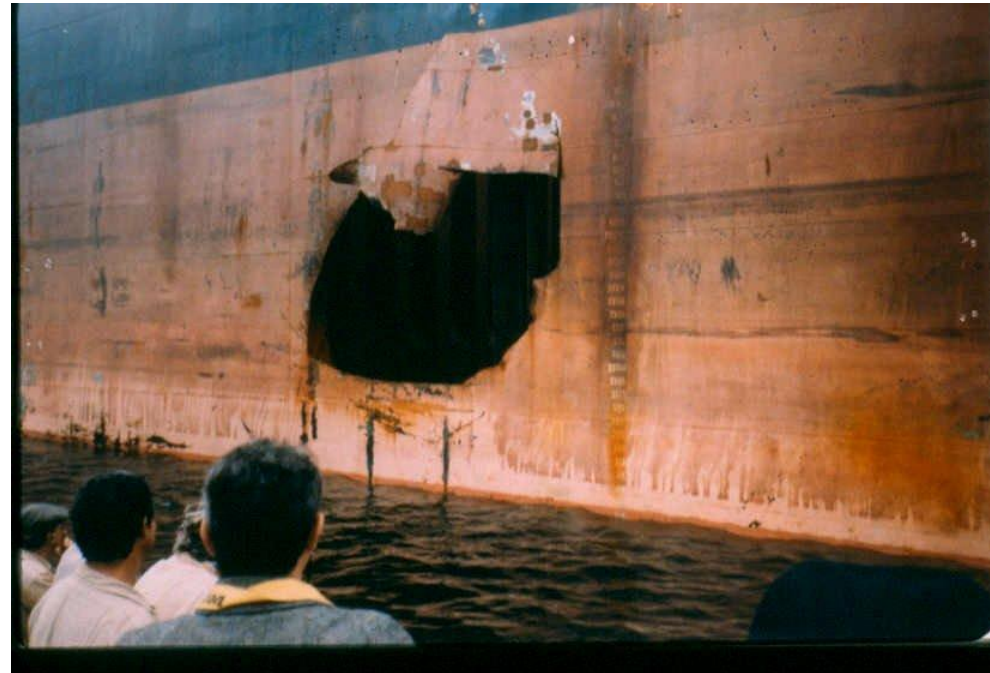
HE HENG
Source NACKS SHIPYARD

Technical structural challenges

- **First generation: lamellar tearing at bulkhead foot**
solved by steel plate testing requirement (Z grade plates)
- **Hatchcoaming/hatchcover stiffnesses: hold tightness**
solved by hatchcoaming deformation computations
- **Ballast in cargo tanks: sloshing and damages**
solved by model tests and upper tank shape design
- **Fatigue cracks and domino effect: shell brittle fracture**
solved by stress computations, fatigue and crack propagation
- **Fast loading by gravity (16,000 t/h): bottom pressure**
solved by R&D and impact structural response computation

Technical structural challenges

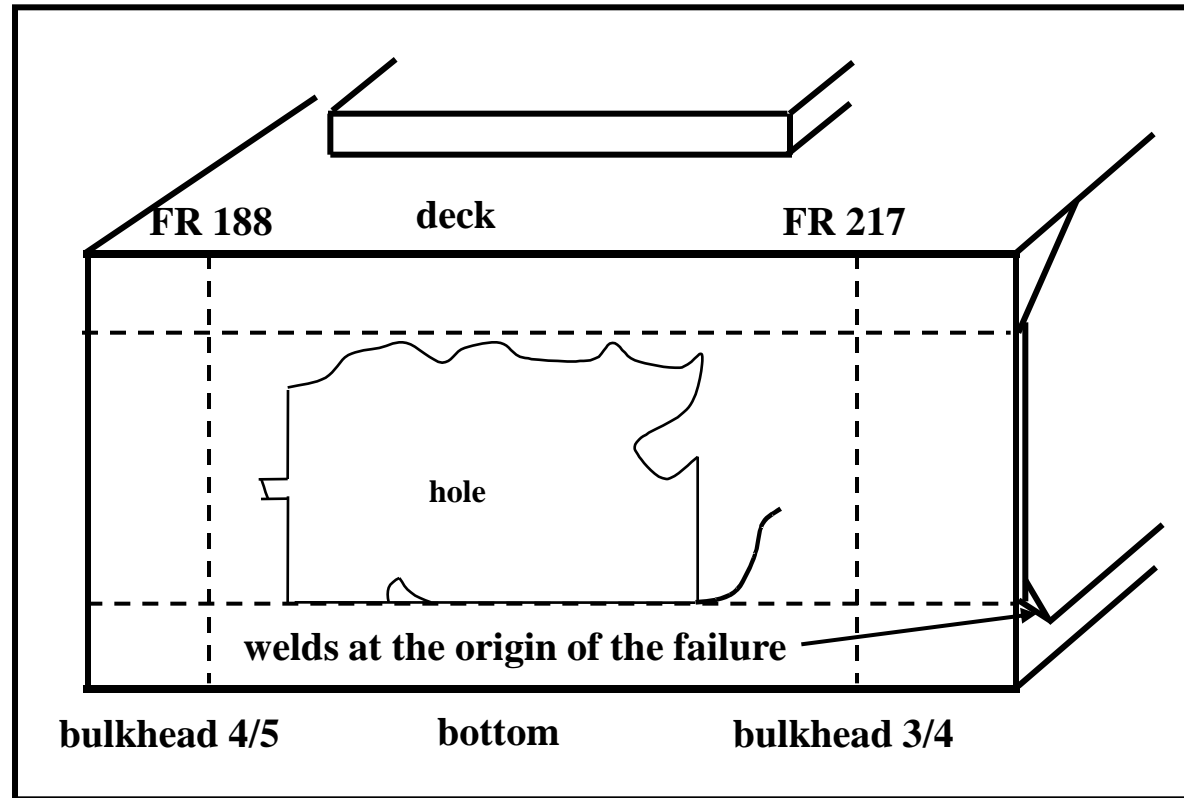
Resulting damage



Technical structural challenges

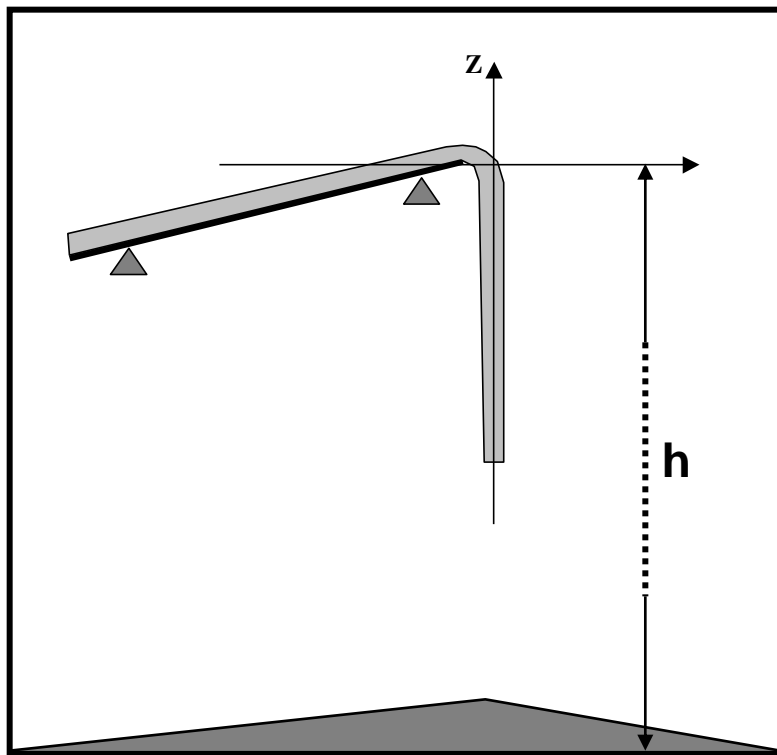
Fatigue cracks
Domino effect

Resulting damage



Technical structural challenges

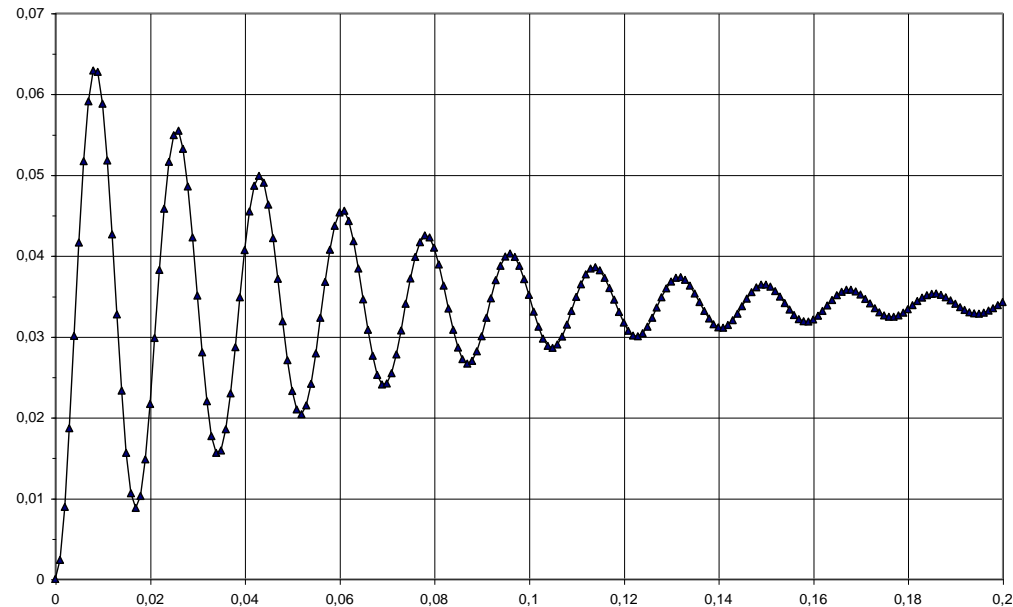
Loading process



16,000 t/h

$h = 26 \text{ m}$

Plate dynamic response



Amplification factor / static = 1.85

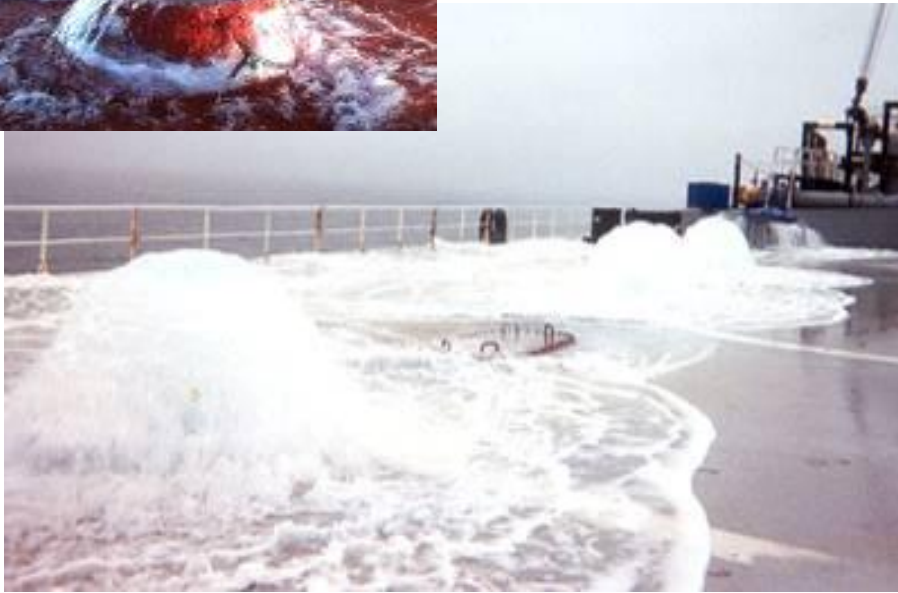
Operational safety

- **Green water on fore deck: ship losses**
solved by R&D and new rules for fore part and monitoring
- **Ballast water exchanges: stability, crew safety**
solved by computation, operational procedures

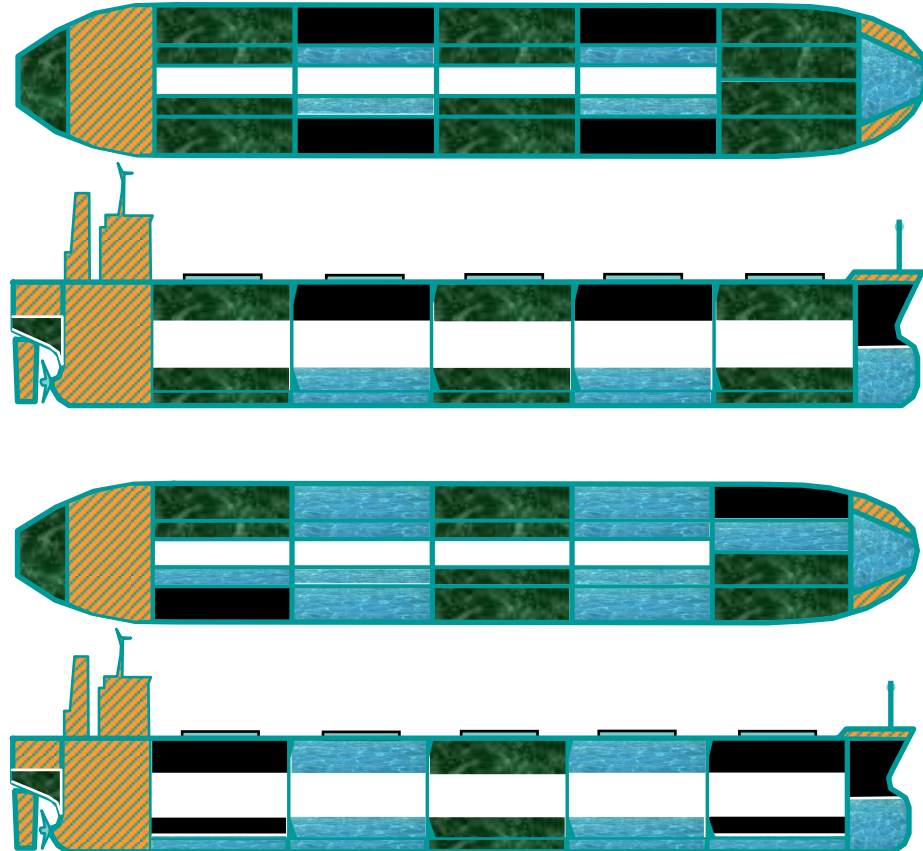


Water ballast exchange

Flow through



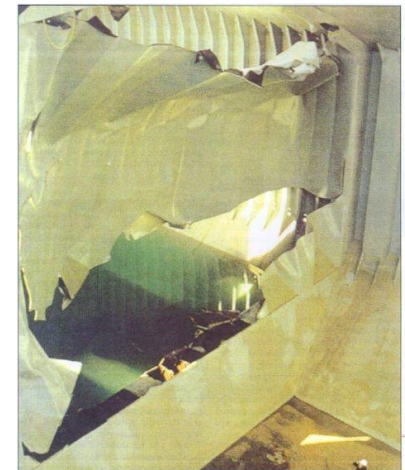
Sequential exchange



Green water on fore deck



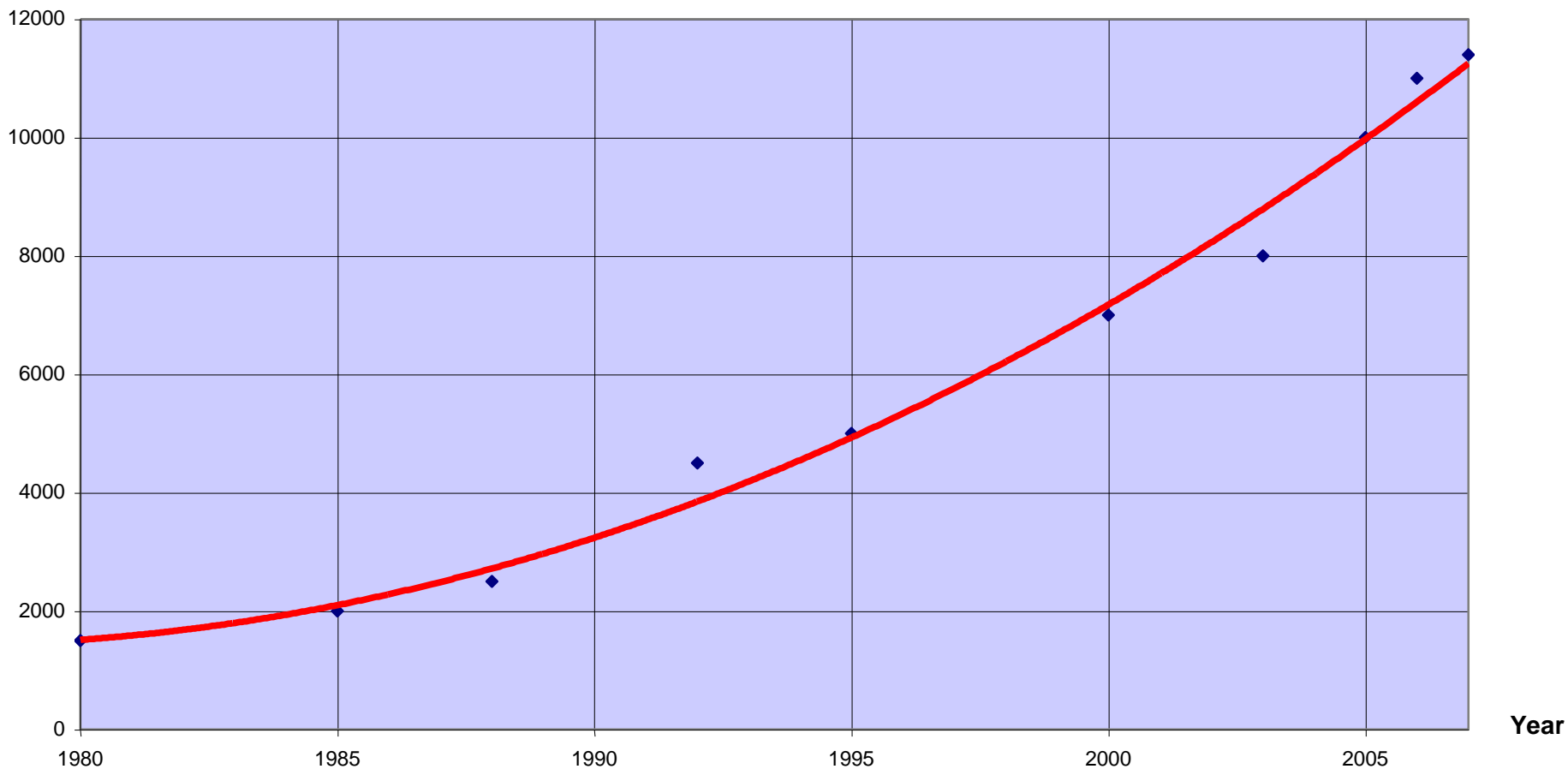
1. Hitting of a strong wave ahead
2. Shipping of green water
3. Damage of the first hatch cover, water ingress in hold
4. Negative trim, cargo fluidisation, sloshing
5. Damage of the hold nb 1 / nb 2 bulkhead →
6. Flooding of the hold nb 2, stability loss
7. Ship capsizing



CONTAINER SHIPS

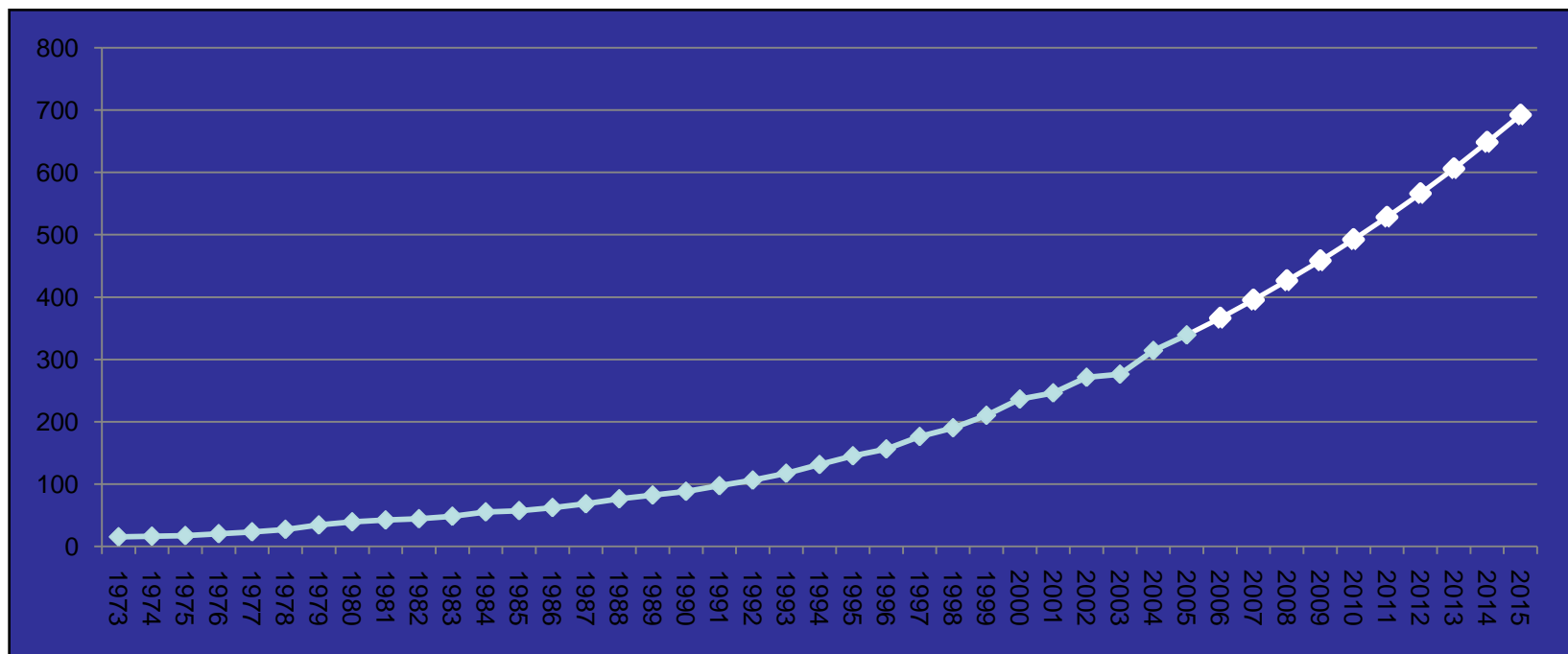
Container ship evolution from 1980 to 2007 Maximum capacity versus years

Capacity in TEUs



projects of 12,500 TEUs

Annual growth in the 9% order was expected before the economic downturn.



CONTAINER SHIPS

10,960 TEUS container ship

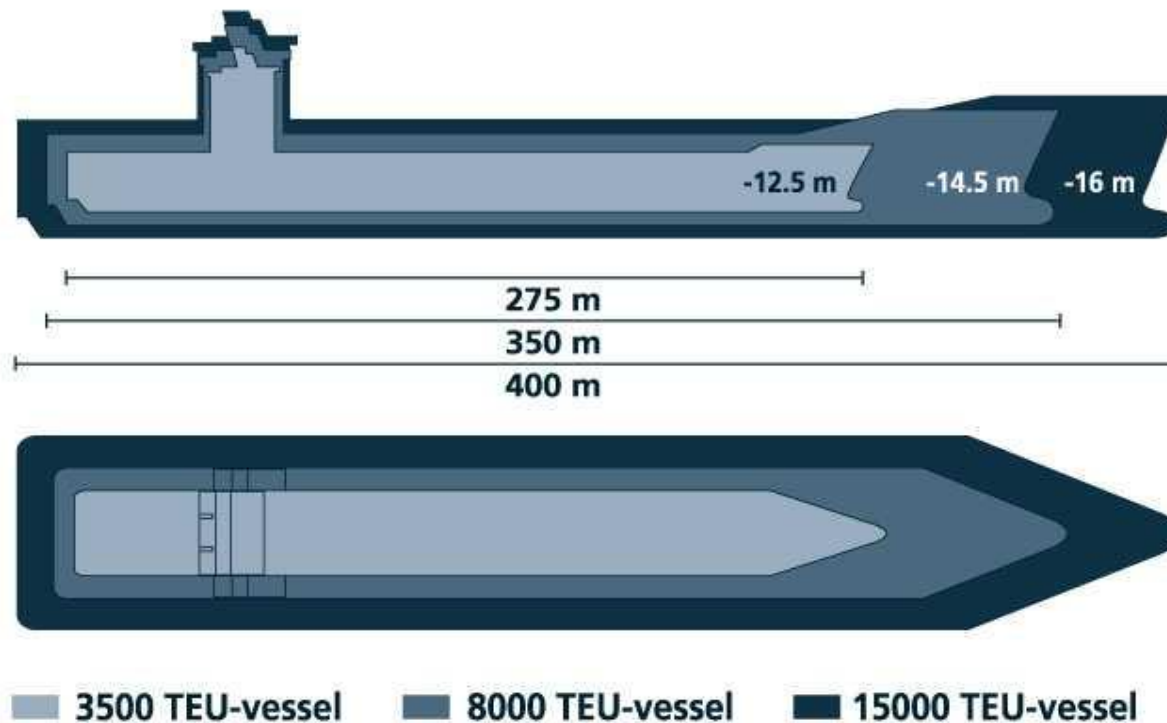


(c) Boris Paulien

L = 346,5 m B = 43,2 m T = 15 m V = 25 knots

Big Box Ships

Ever Larger Vessels



15000 TEU
±25 wide 7 high



8000 TEU
±17 wide 7 high



3500 TEU
13 wide 4 high





Representative ship dimensions



Ship	Year	TEU	Loa (m)	Beam (m)	Draft (m)	Speed (kn)
CMA-CGM Hugo	2004	8 200	334.1	42.8	14.5	
DSME	2009	9 000	347	45.2	15.5	24.3
HHI	2009	11 400	363	45.6	15.5	
DSME	2009	13 000	365.5	51.2	14.0	

*Power is about 72 000 kw to 80 000 kw with 2-stroke low rpm
 12 – 14 cylinders Diesel engines
 Operating draft between 14 m and 15 m
 Air draft about 64.5 m*



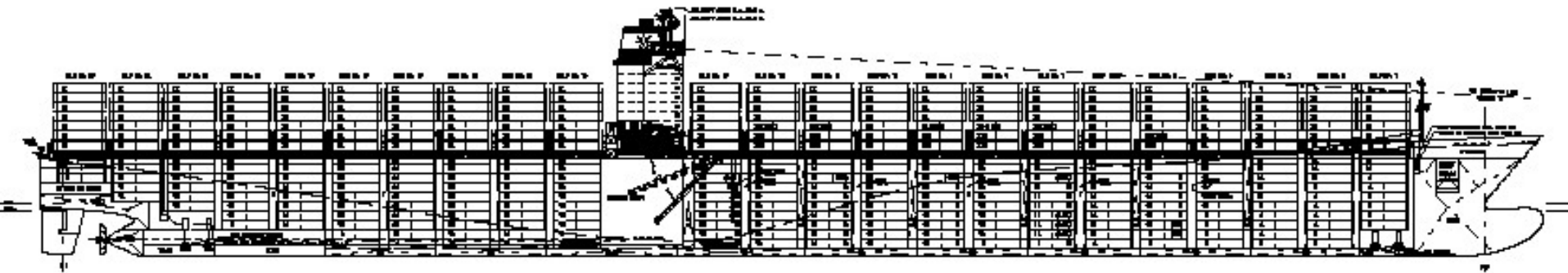


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M/V EMMA MAERSK



LE RENDEZ-VOUS DE CANNES



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In order to handle much larger vessels and consignment sizes terminals must both expand and make better use of existing facilities

In North Europe, consignment sizes are averaging nearly 2700TEU for 6000TEU+ sizes. For very large vessels, up to 5000TEUs have been handled at single port calls

These increases will be noted in all major front rank ports

- Large and slender hullform boxships have relatively small bending and torsional rigidity
- Therefore, the natural frequencies of hull girder vibrations are relatively small (large natural periods)
- High forward speed of container ships gives increases the wave encounter frequency (smaller wave encounter period)
- Consequently, dynamic phenomena which are second order for average size vessels may become of high importance for ULCS
- Main issue: vibratory structural response and associated fatigue damage caused by whipping and springing
- Extrapolation of existing designs to ULCS dimensions risky business?

* Ultra Large Container Ship: 10,000+ TEU

- Whipping is a transient phenomenon characterised as hydrodynamic impact enforcing high frequency hull girder bending stresses (vibration)
 - Increased sagging and hogging wave bending moment (stress amplitude)
 - Increased fatigue loading (small range high frequency damped cycles and low frequency stress range)
- Whipping generally occurs in head seas when sailing severe sea states; main vibration mode is vertical bending
- Springing is a resonant phenomenon characterised as small range high frequent bending stresses which are added to the large range wave frequent bending stresses
 - Increased fatigue loading (small range high frequency cycles)
- Springing generally occurs in quartering seas when sailing in non-severe sea states (waves with small period have limited height); main vibration modes are torsional bending, vertical bending and horizontal bending

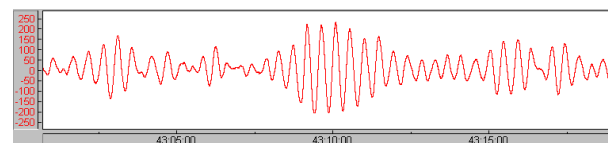
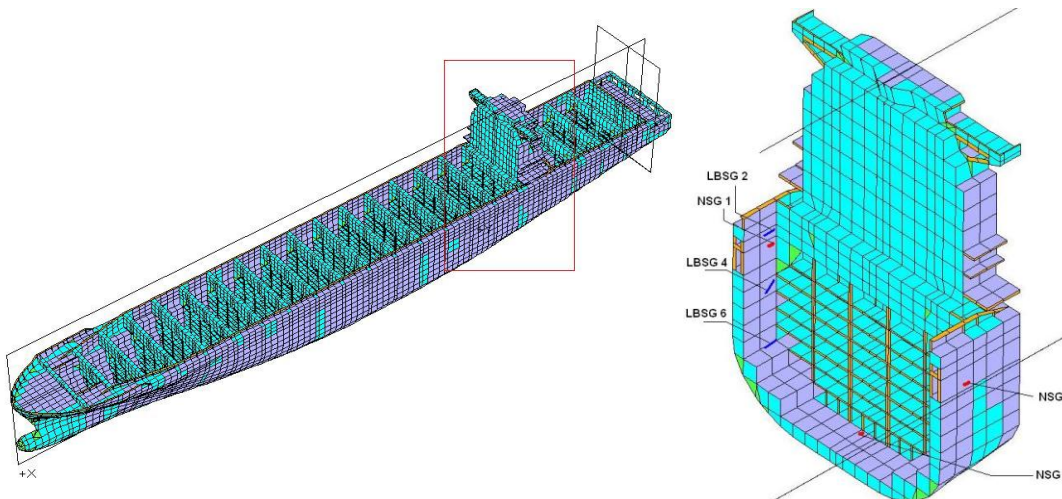


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Full scale measurements: Lashing@Sea



LE RENDEZ-VOUS DE CANNES

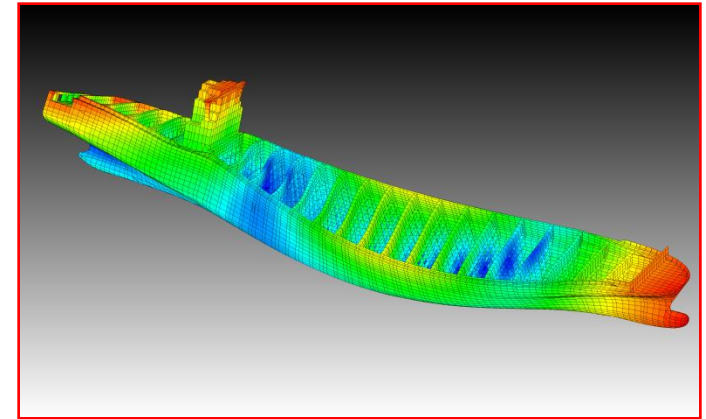
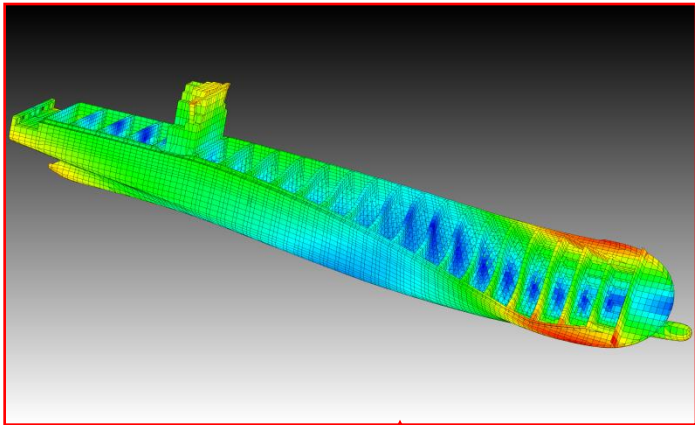


Transverse accelerations

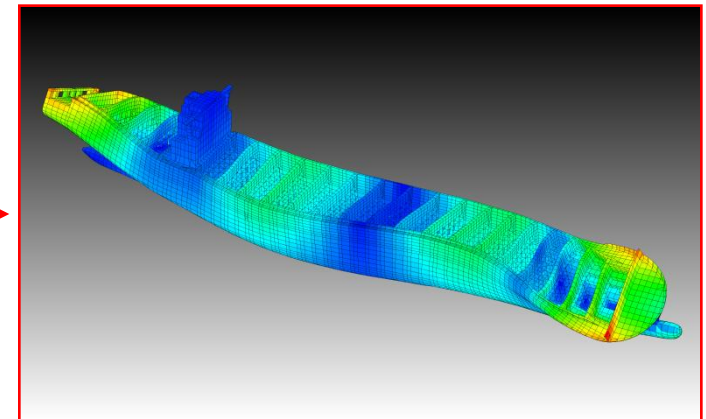
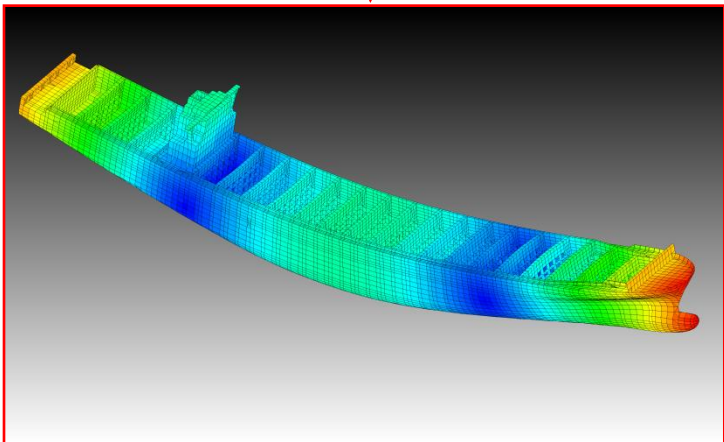
CMA CGM Rigoletto – 9400 TEU – BV Class

Measurement of hull stresses and container accelerations

Results:



Frequencies	
Mode	(Hz)
torsion	0.366
flexion	0.496
torsion	0.499
torsion	0.899



ULCS: What are the findings?

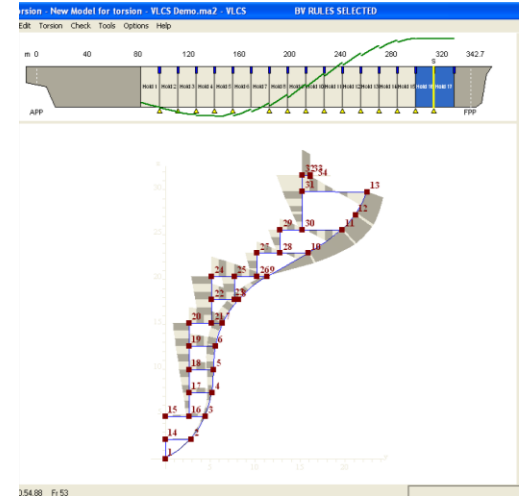
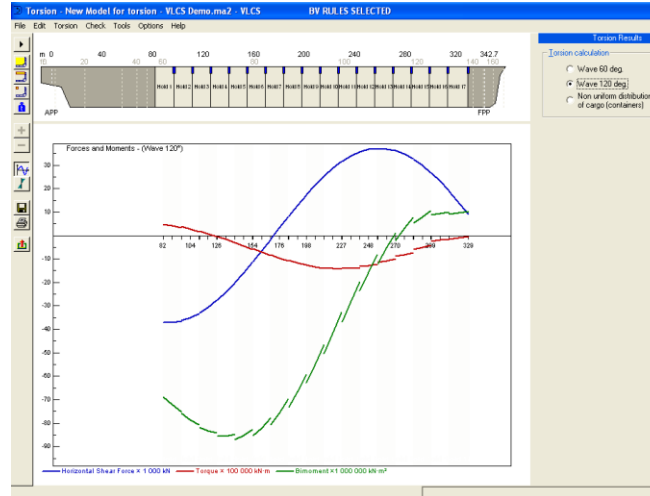
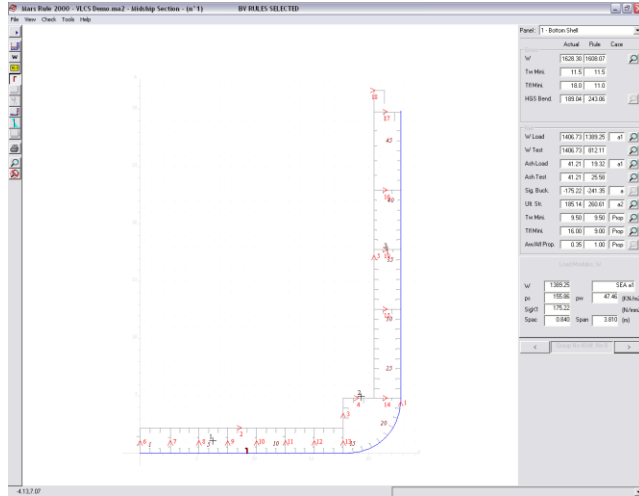
- Whipping can cause an increase in total vertical bending moment of about 20%
- The whipping induced increase in fatigue damage during the vessel lifetime has been found to be of the order of 3 to 5%
- The springing induced increase in fatigue damage during the vessel lifetime has been found to be of the order of 4 to 10%
- Consequences for the design of ULCS
 - The hull girder ultimate strength check will need to take into account the increase in dynamic hull girder loads
 - Increased attention required for the design of fatigue sensitive structural details (hatch corners, longitudinal connections, etc.)
- Effects of whipping and springing will become more important for new designs for container ships of over 400 m in length (over 13,000 TEU)



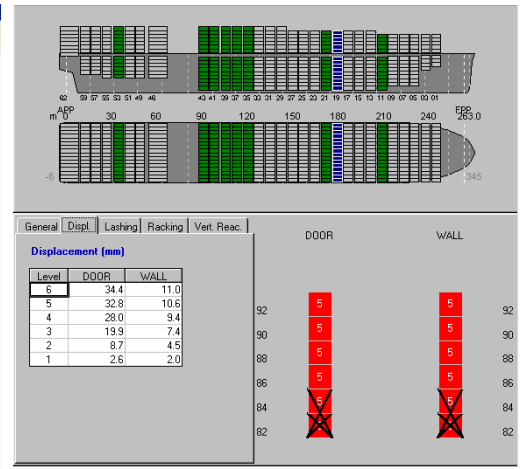
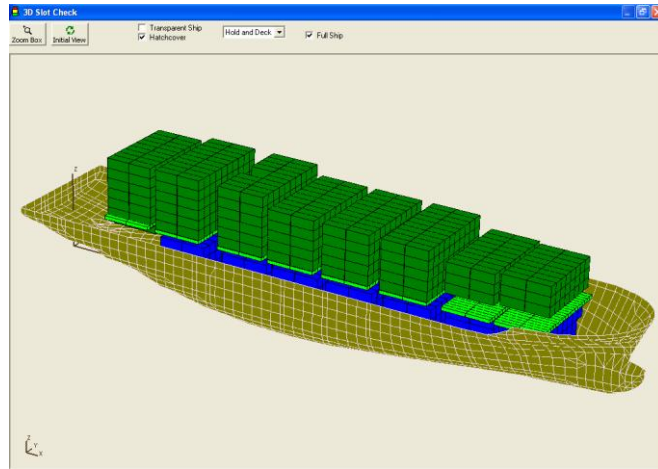
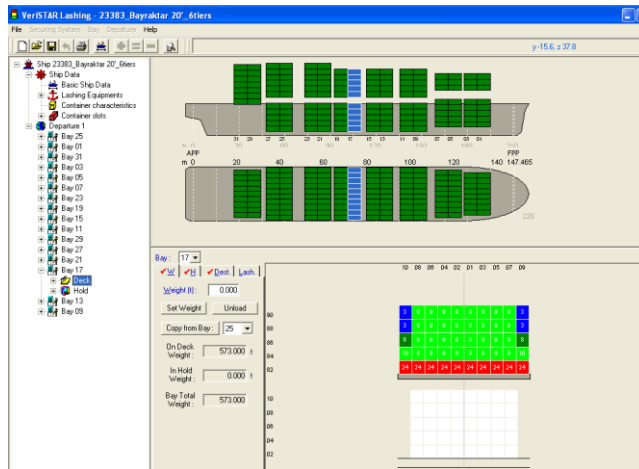
High quality user friendly tools for efficient design



LE RENDEZ-VOUS DE CANNES



MARS2000: longitudinal & ultimate strength, transverse bulkheads, torsion, fatigue



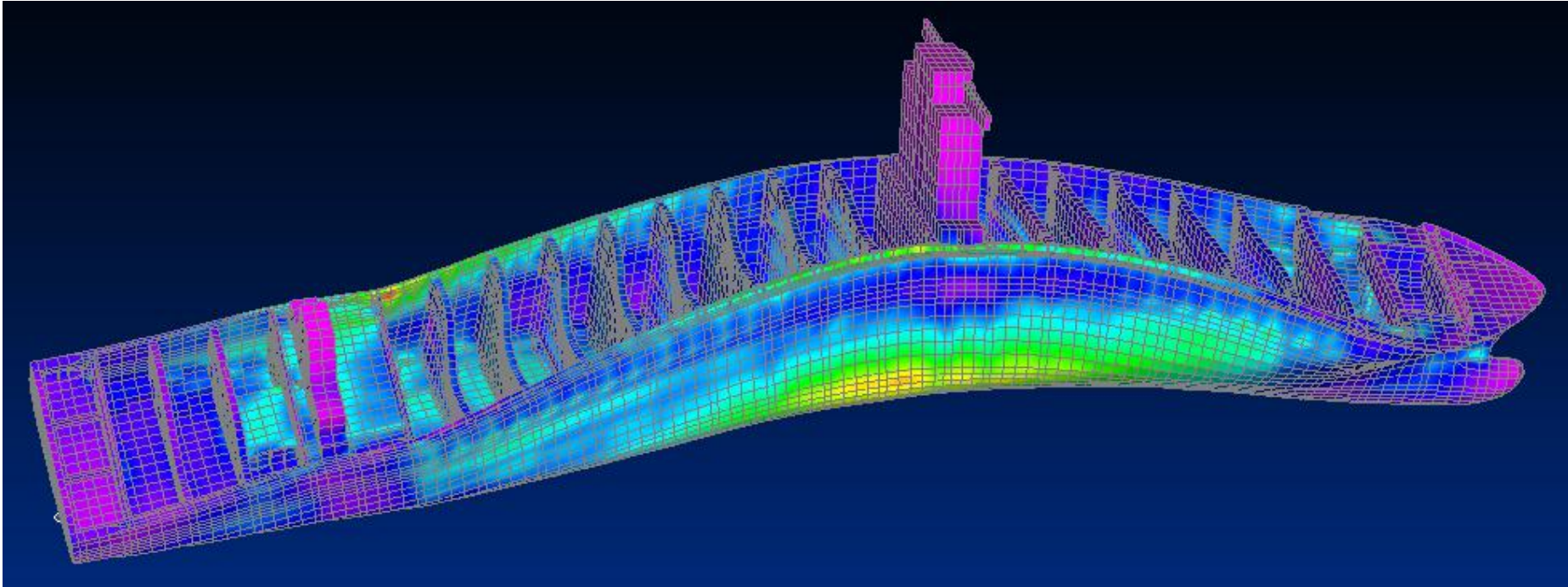
VeriSTAR LASHING: verification and optimisation of stackweight and lashing equipment



Direct Ship Analysis



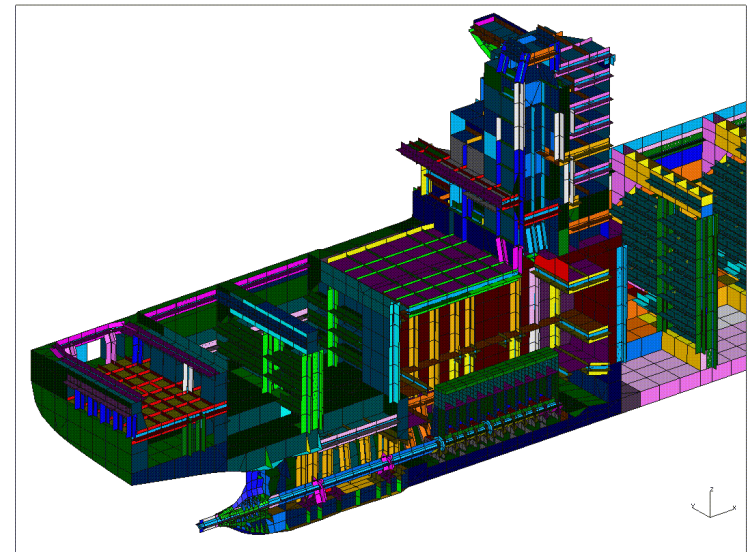
- Necessary for large container ships...



13,000+ TEU



- Flexible hull structure due to open box holds (vertical bending and torsion) and weight optimisation (FE calculations)
- High power output for high sustainable service speed
- Main engine and crankshaft stiffness are relevant parameters due to specific architecture of main engine
- Hydrodynamic design aspects for single screw high powered ships (vibrations excitations, cavitation erosion)
- Direct coupling between line shafting and crankshaft



Technical structural challenges

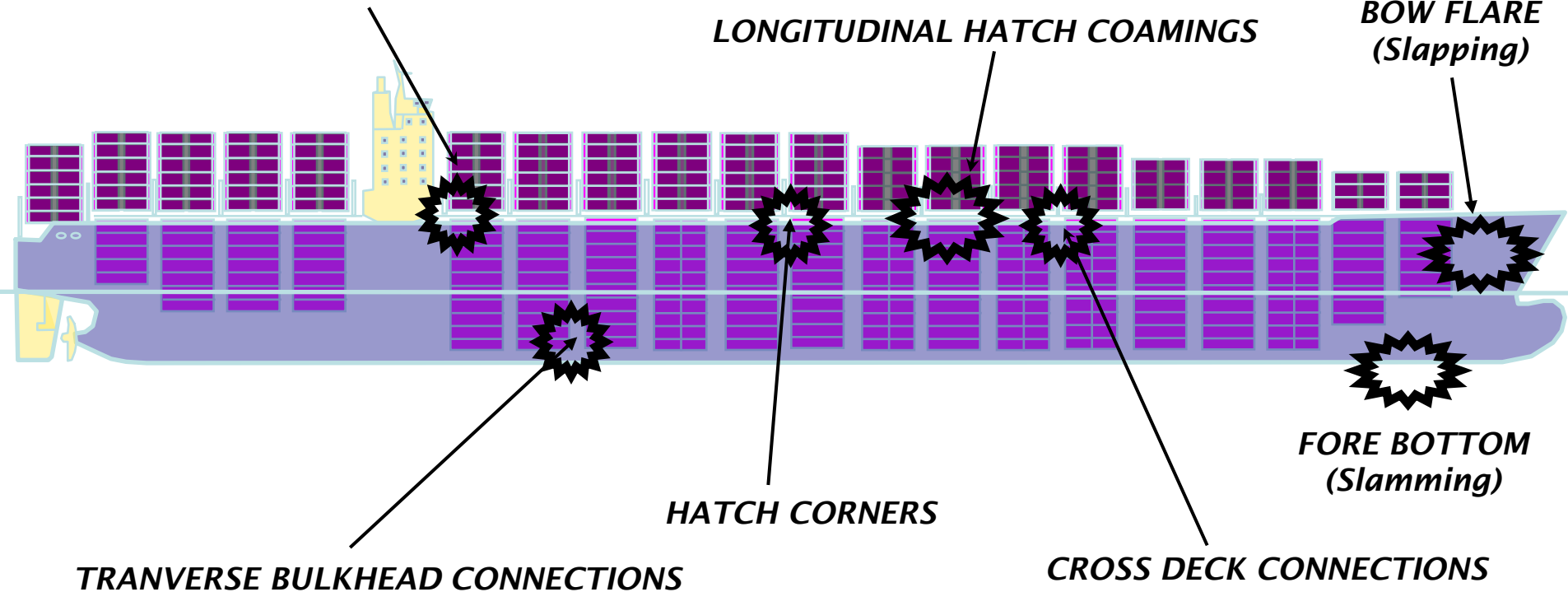
- **Large open deck:** torsion, fatigue in hatch corners
solved by measurements at sea, then stress computations
- **Wave impacts:** slamming, slapping, green water
solved by hydrodynamic computations, hull monitoring
- **Dynamic wave loads:** hull girder springing, whipping
solved by stress computation and fatigue verification
- **Motion accelerations:** on deck container lashing
solved by load and stress computations, lashing design
- **Propulsion power:** shaft alignment, rudder erosion
solved by elastic alignment, rudder shape and material

Structural critical areas

HATCH COAMING/CASTLE CONNECTION

LONGITUDINAL HATCH COAMINGS

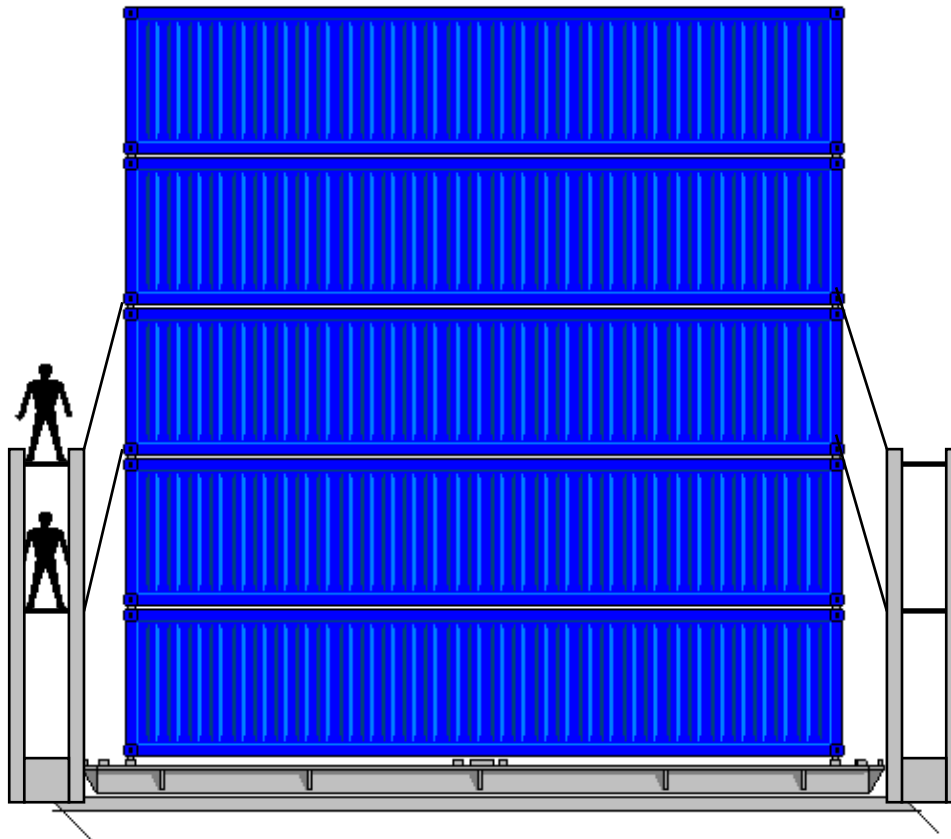
*BOW FLARE
(Slapping)*



Container lashing failure



Container lashing innovation



Lashing deck on 2 levels

Advantages:

- Short lashing lines
- 2 workers at the same time
- Easier working conditions

Inconvenient:

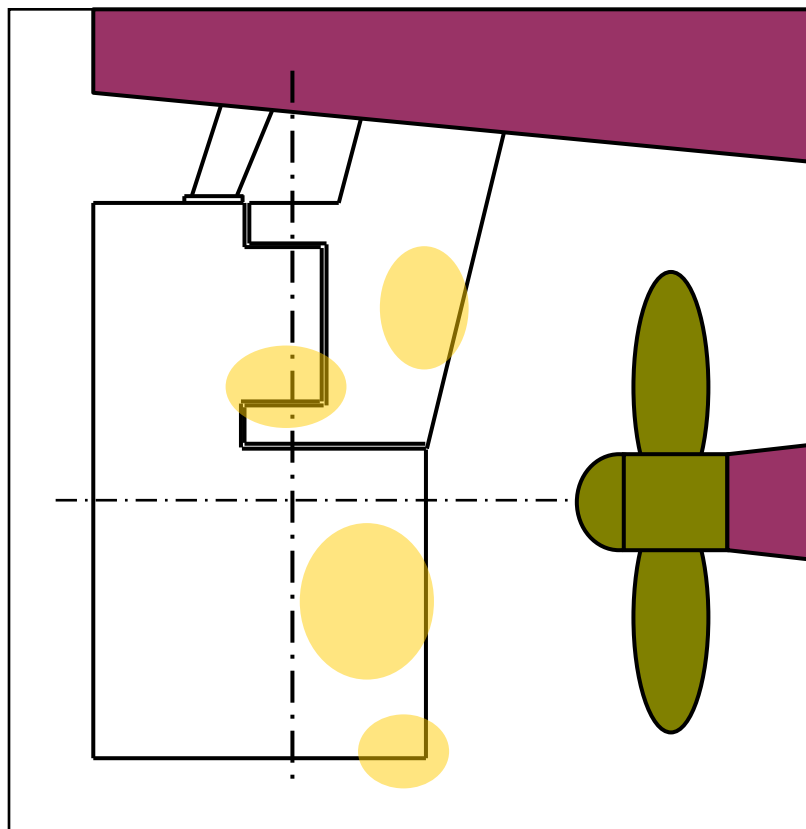
- Heavier equipment

Rudder erosion

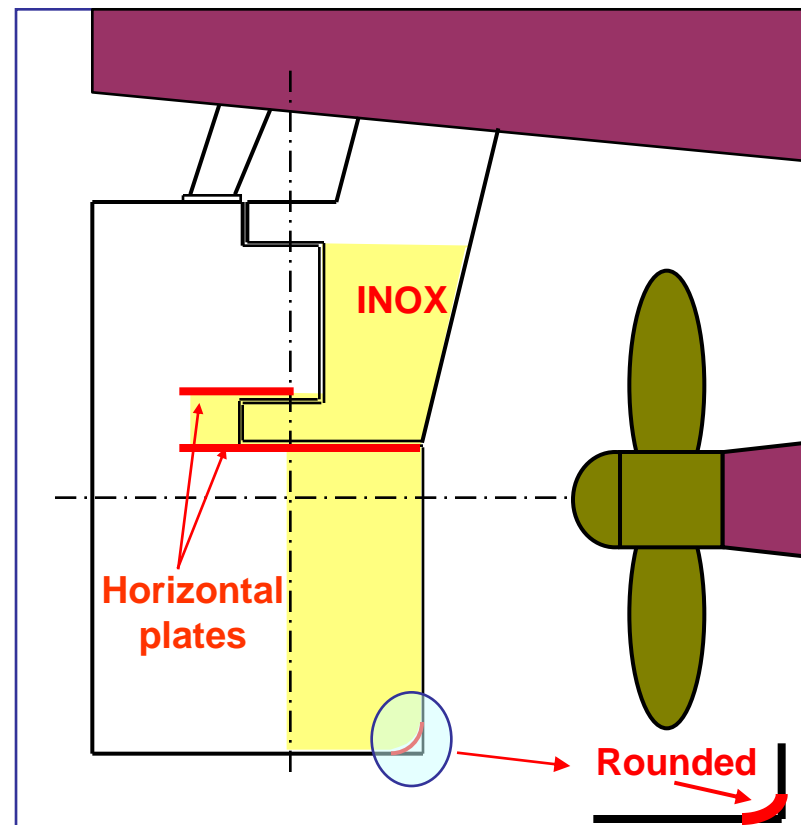


Rudder erosion

Concerned areas



Proposed solutions



Operational safety

- **Fast speed: collision risk**
solved by manoeuvrability and navigation rules
- **Containers on deck: visibility, green water**
solved by monitoring, bridge position
- **Containers on deck: parametric rolling**
solved by R&D, computation and navigation rules

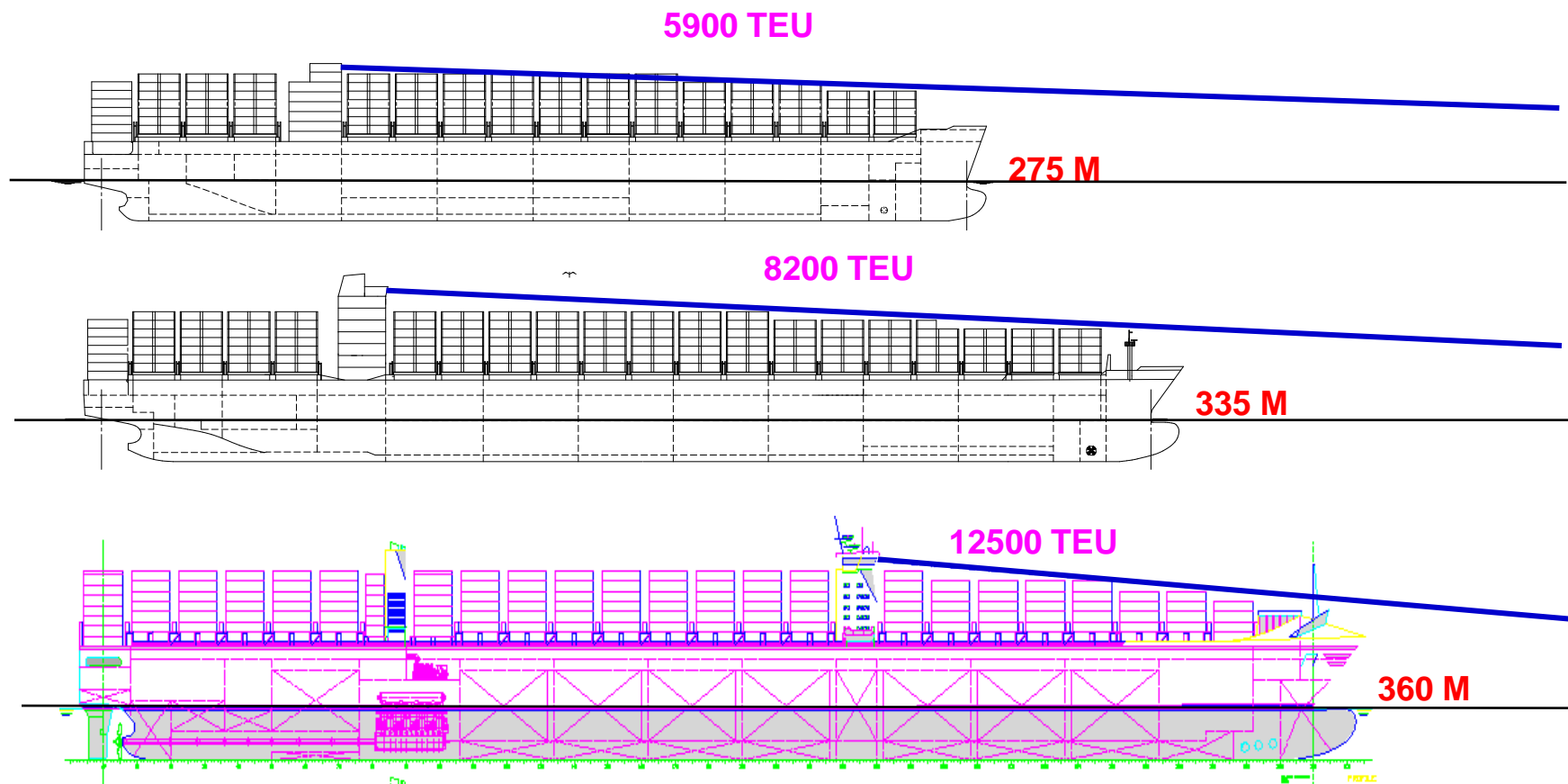


CONTAINER SHIPS

Visibility from bridge



Visibility from bridge



CONTAINER SHIPS

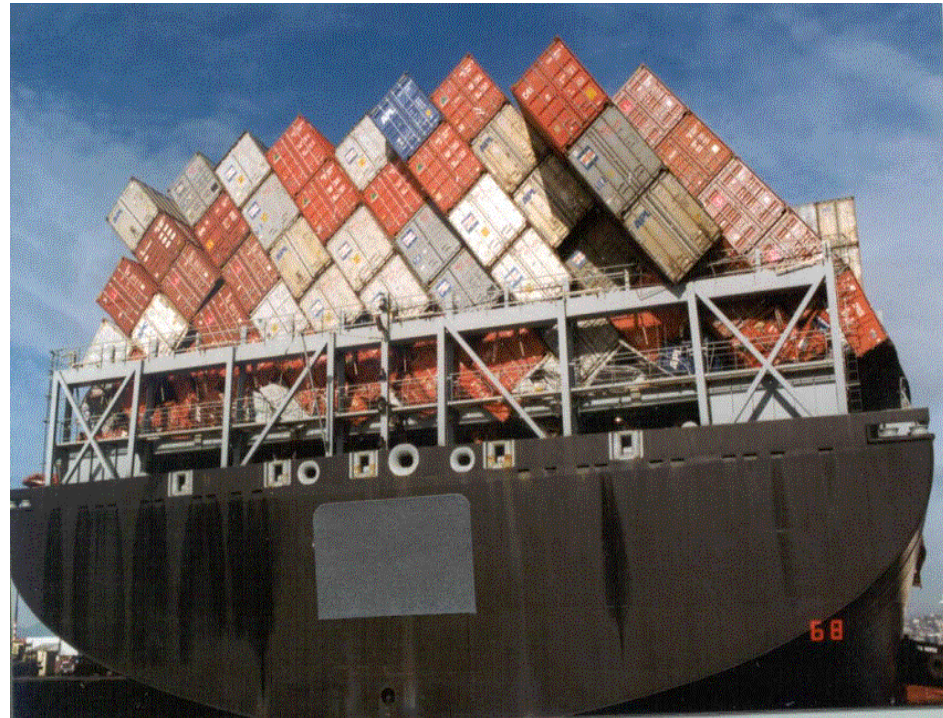
Shipping of green water



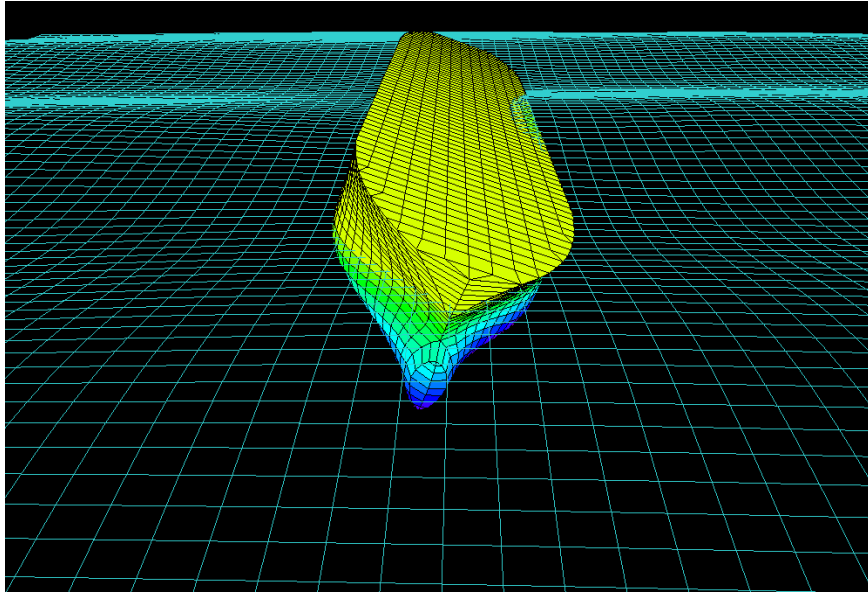
Shipping of green water effects



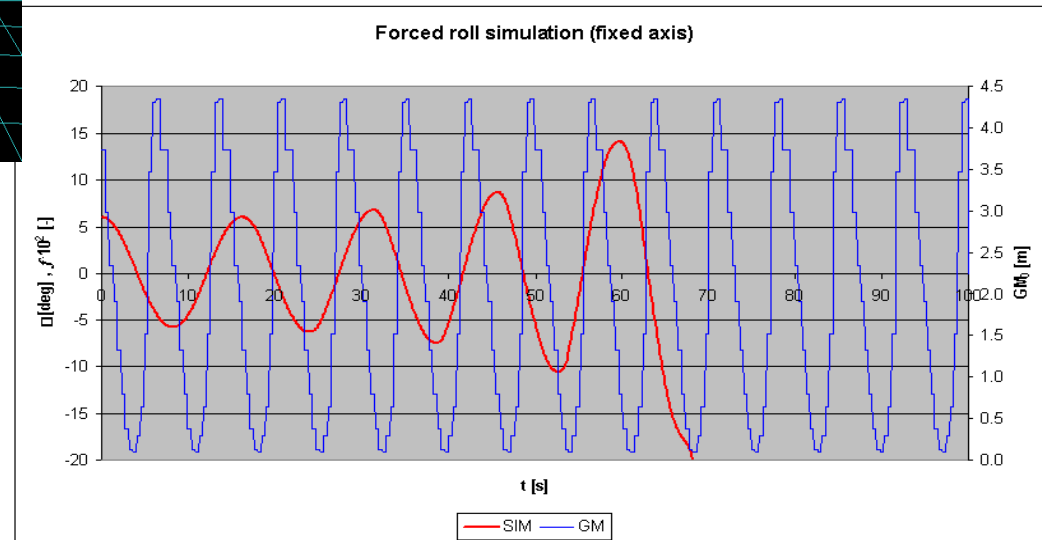
Parametric rolling effects



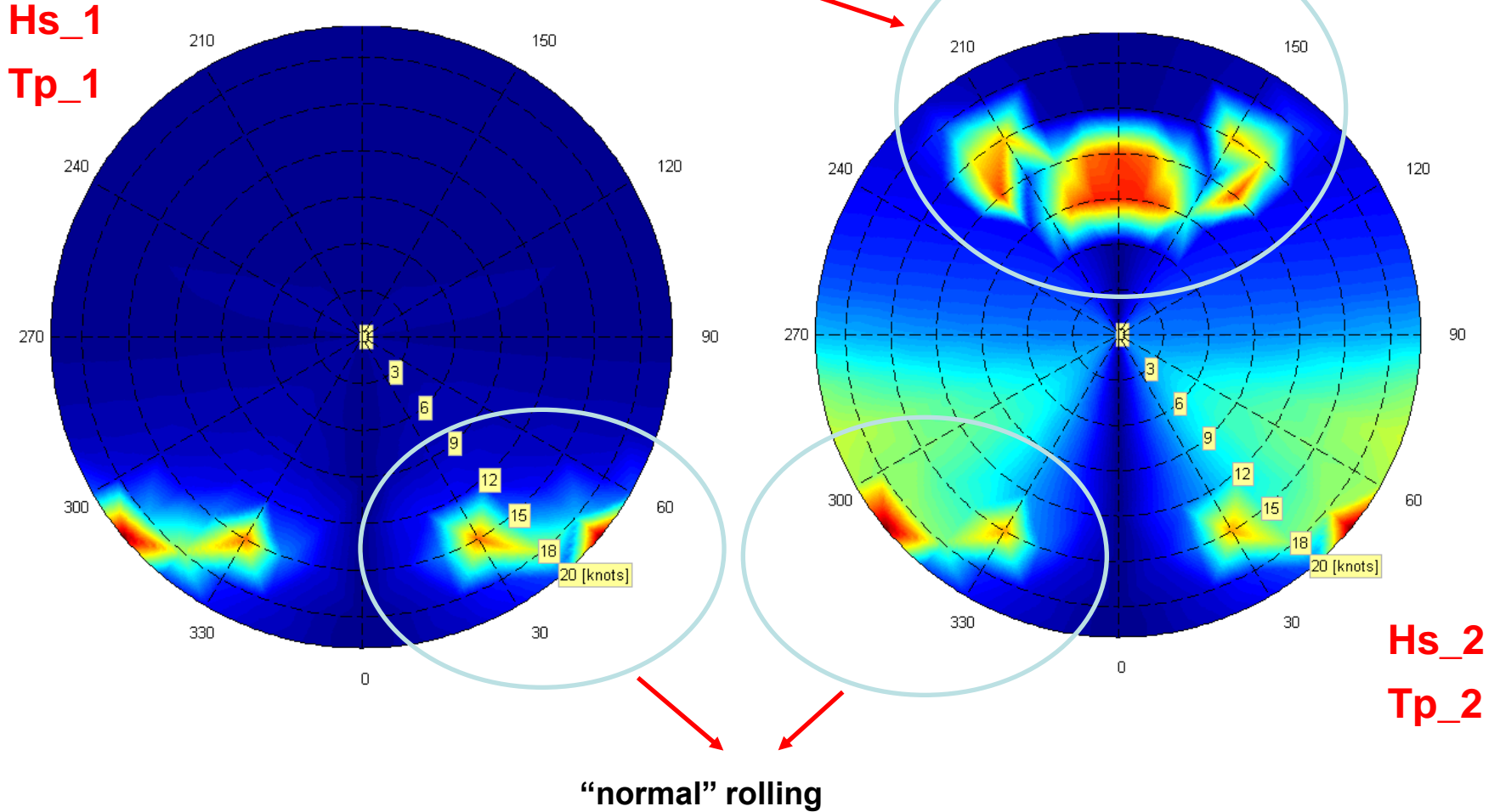
Parametric rolling computation



Roll time history

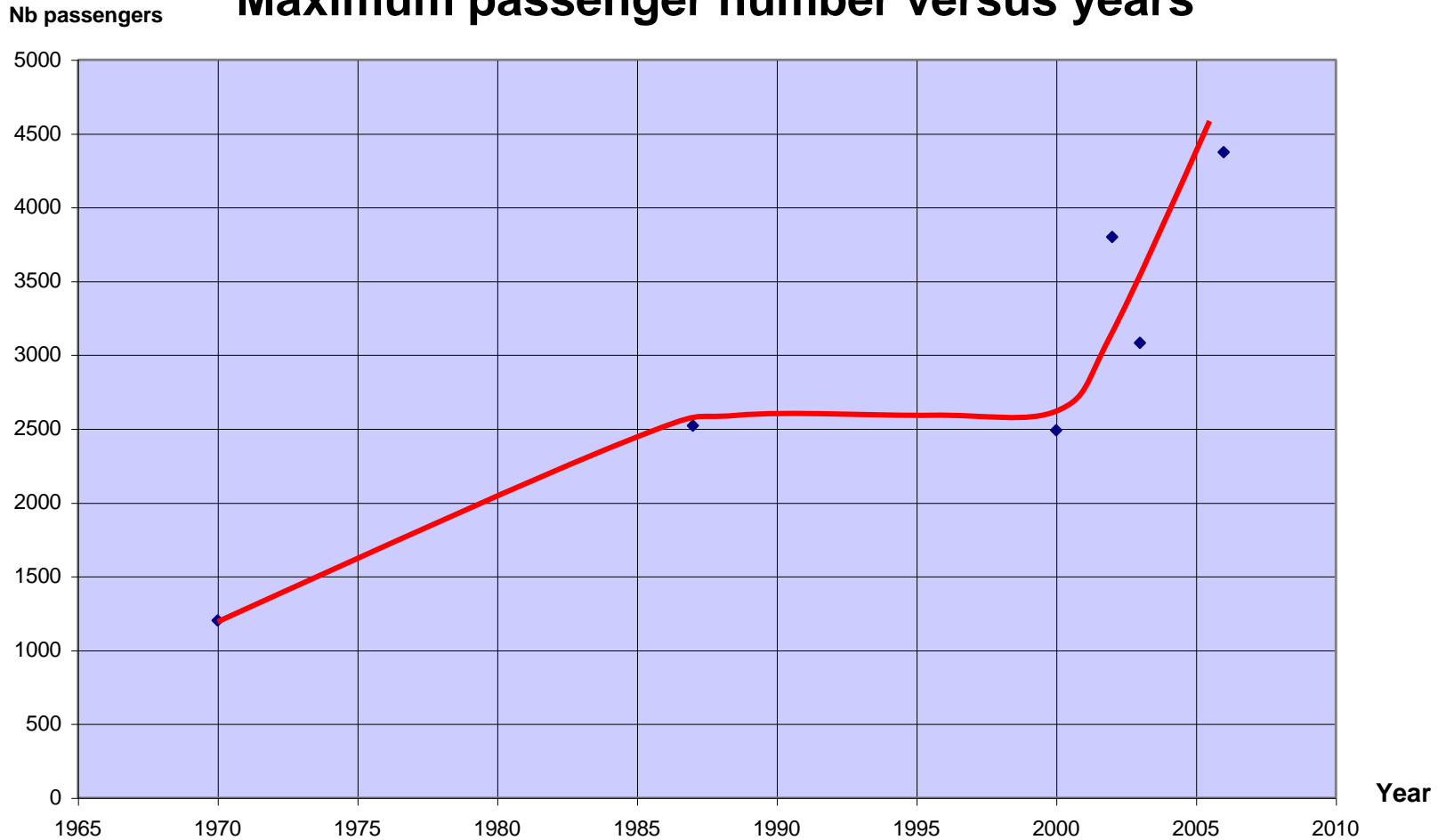


Parametric rolling risk prediction



CRUISE LINERS

Cruise liner evolution from 1970 to 2006 Maximum passenger number versus years



project of 5,600 passengers

CRUISE LINERS

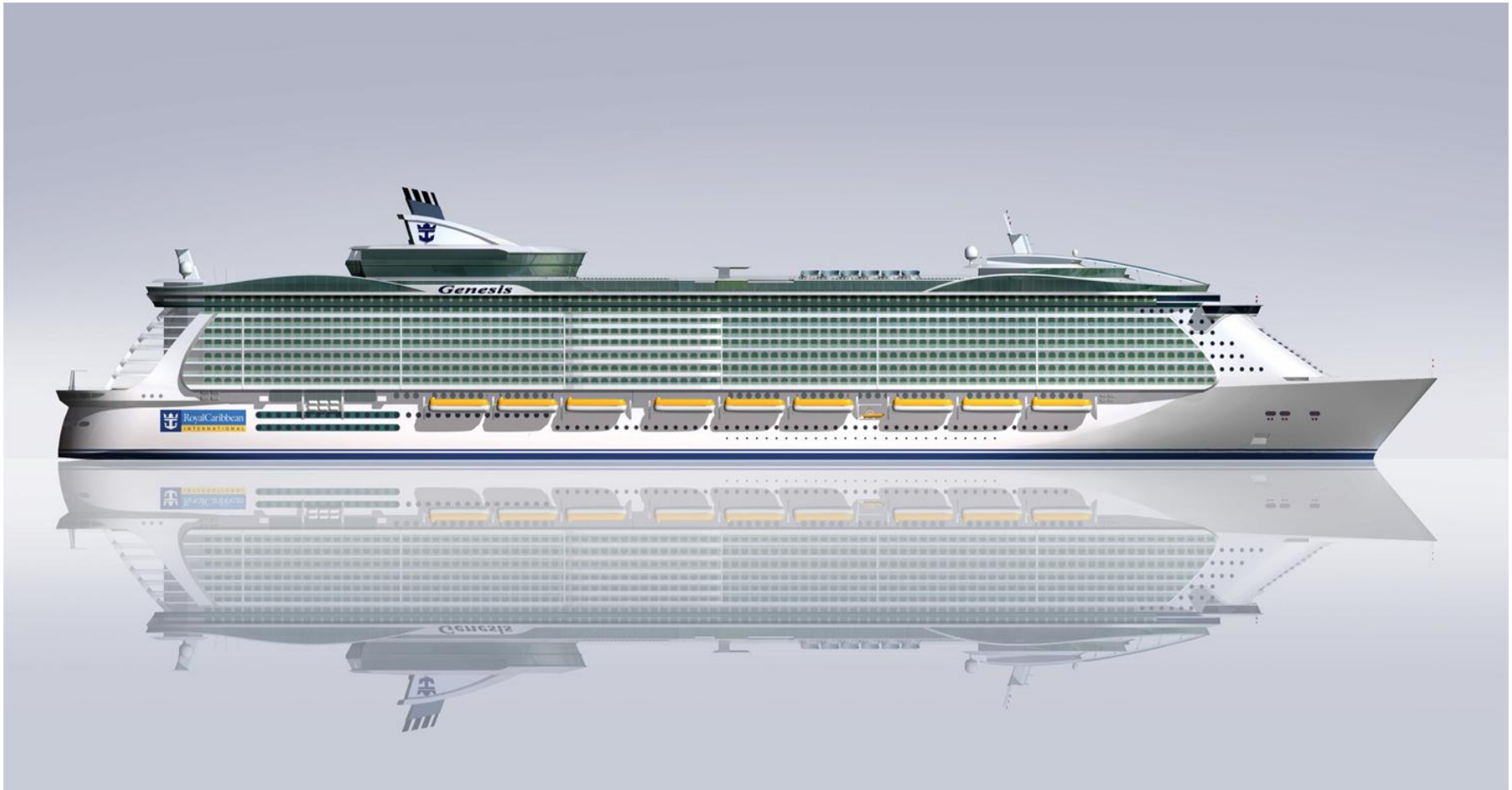
Norway: 2000 passengers L = 315 m



Queen Mary II
3080 passengers
L = 345 m

CRUISE LINERS

Genesis project: 5600 passengers L = 360 m



Technical structural challenges

- **Superstructures:** hull girder deformation loads solved by structural stress computations
- **Large wide spaces:** structural discontinuities solved by structural behaviour computations
- **Large shell opening:** structural discontinuities solved by structural behaviour computations
- **Passenger comfort:** reduced vibration, noise solved by structural behaviour computations
- **Propulsion:** large flexibility needed solved by PODS

CRUISE LINERS

Large superstructures submitted to hull girder deformations



MSC SERENATA 133.000 GT 1.650 Pax Cabins Over-Panamax size - May 2009

Wide space: commercial centre



Wide open spaces



Theater

Main stair



CRUISE LINERS

Passenger comfort

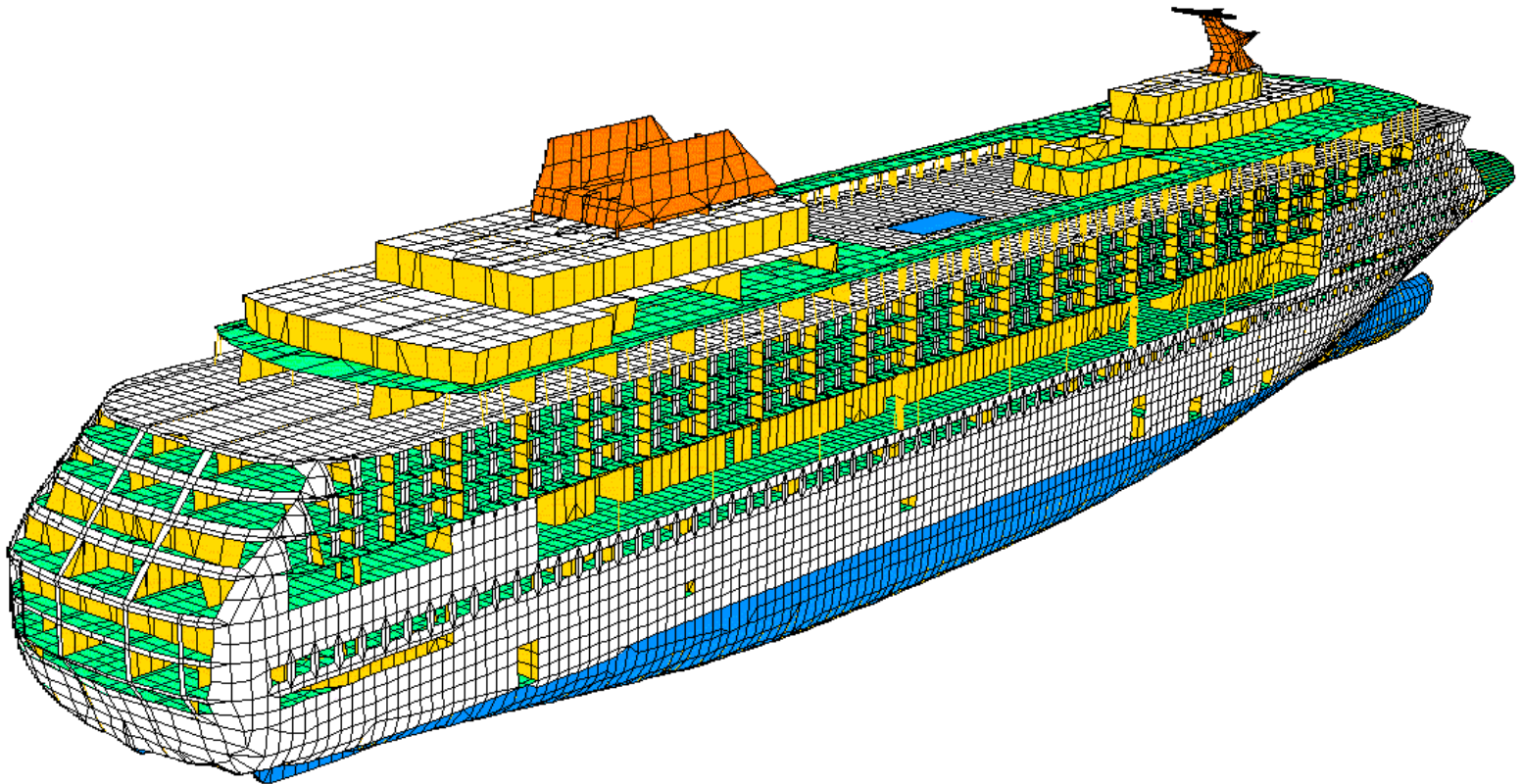


Bar and Restaurant

Cabin room



FE model for vibration and noise prediction computation



CRUISE LINERS

Propulsion flexibility



Queen Mary II PODS

CRUISE LINERS

Operational safety

- **Stability: ship capsizing**
solved by damage stability computations
- **Health: air conditioning, water, food**
solved by procedures, maintenance, audits
- **Environment: garbage and sewage**
solved by design and equipment
- **Fire: detection, protection, fighting**
solved by specific rules and fire propagation computations
- **Evacuation: number of passengers and panic**
solved by specific equipment and computer simulations

Lost of stability consequences



RoRo/Ferries losses

from 1987 to 2002

accidents 9

capsizings 7

victims 3 644

Contamination by air conditioning



Risk of legionella

CRUISE LINERS

Contamination by water



warm water

legionella

cold water

pseudomonas

CRUISE LINERS

Contamination by foods



CRUISE LINERS

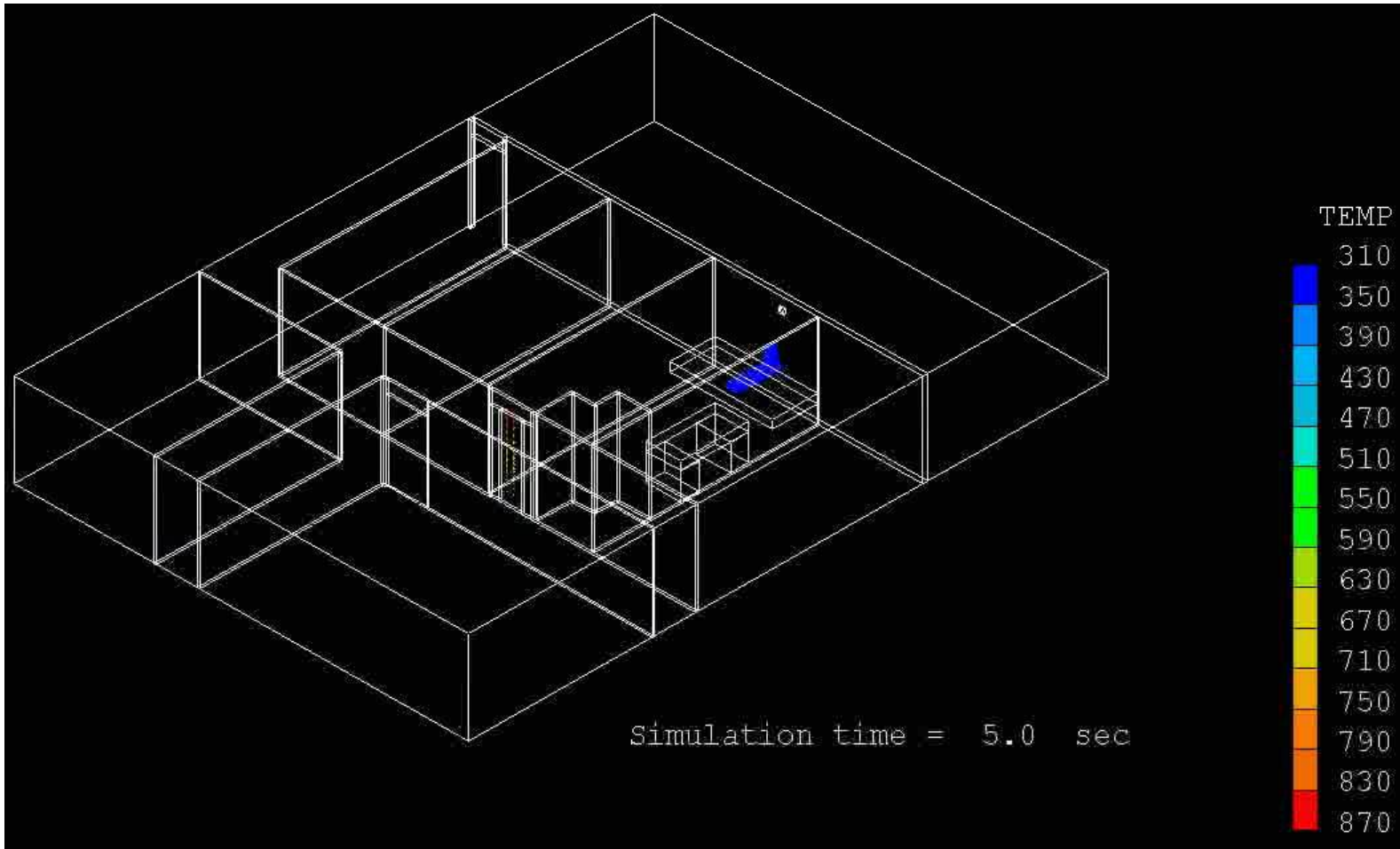
Waste quantities

Cruise liner of 3,000 passengers

Type of waste	kg or liter/person/day	tons or m ³ /week
Plastic	0.1	2.1 t
Paper and pasteboard	1.0	21.0 t
Glass	1.0	21.0 t
Food garbage	0.7	14.7 t
Total solid	2.8	58.8 t
Black water (conventional system)	100	2 100 m ³
Black water (void system)	12	252 m ³
Grey waters	160	3 360 m ³
Wash houses	80	1 680 m ³
Kitchens	90	1 890 m ³
Total liquid	430 / 342	9 030 / 7 182 m³

CRUISE LINERS

Fire propagation simulation



FIRE SAFETY ENGINEERING GROUP

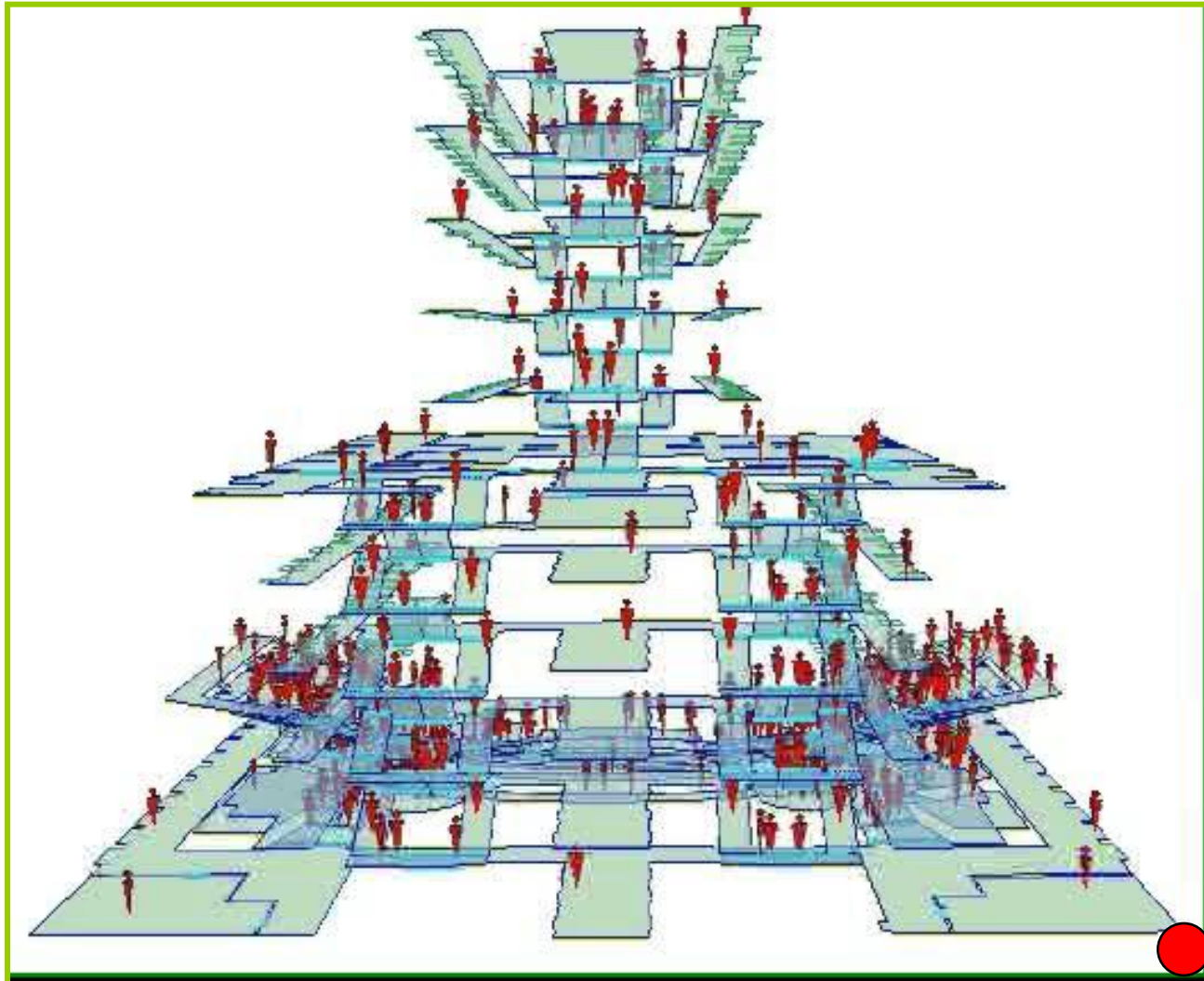
UNIVERSITY OF GREENWICH

Salvage crafts and evacuation training



CRUISE LINERS

Evacuation computer simulation



SYNTHESIS

- **SINCE MAGDALA TANKER (1969)**

All ship structures are verified by structural computations

- **SINCE YEARS 70s**

All ship types have increased in size thanks to R&D and computer progresses

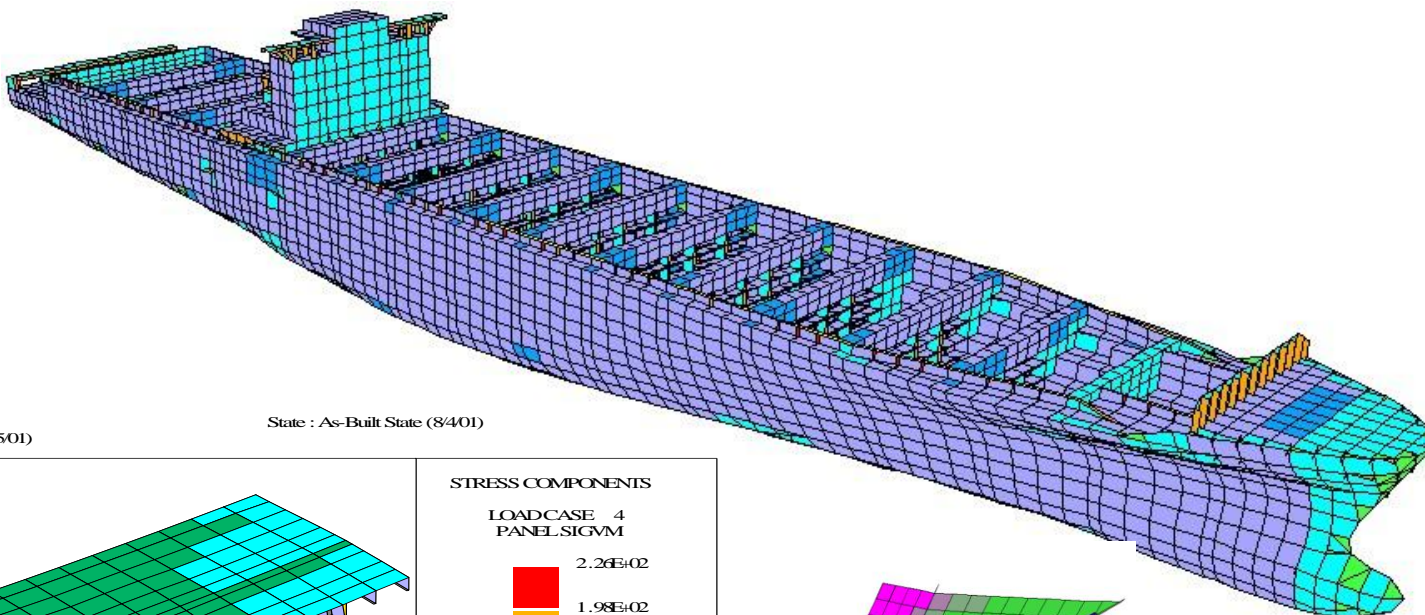
- **TODAY**

Ship designers and operators have efficient tools for calculations and simulations



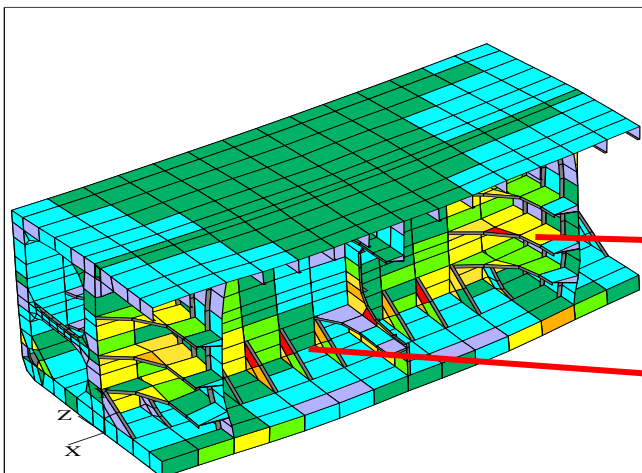
SYNTHESIS

Global and local hull stresses



Ship : 01739S
Model : ch4 (8/15/01)

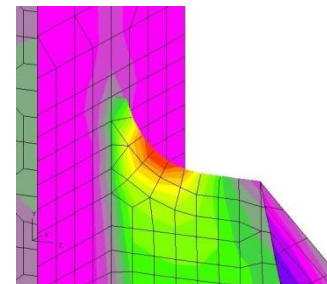
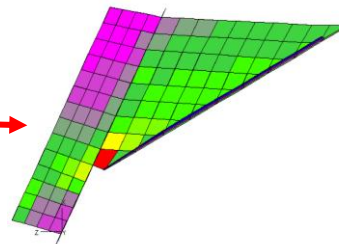
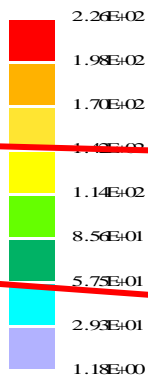
State : As-Built State (8/4/01)



DISPLACEMENTS: LOAD CASE 4:
LC10 GALE BALLAST HEAD, D.S. TROUGH, NEM

STRESS COMPONENTS

LOADCASE 4
PANEL.SIGVM



VeriSTAR

END

Thank you for your attention

LE RENDEZ-VOUS DE L'ASSURANCE TRANSPORTS

Cannes
28th and 29th April 2009



CESAM



LE
RENDEZ-VOUS
DE CANNES